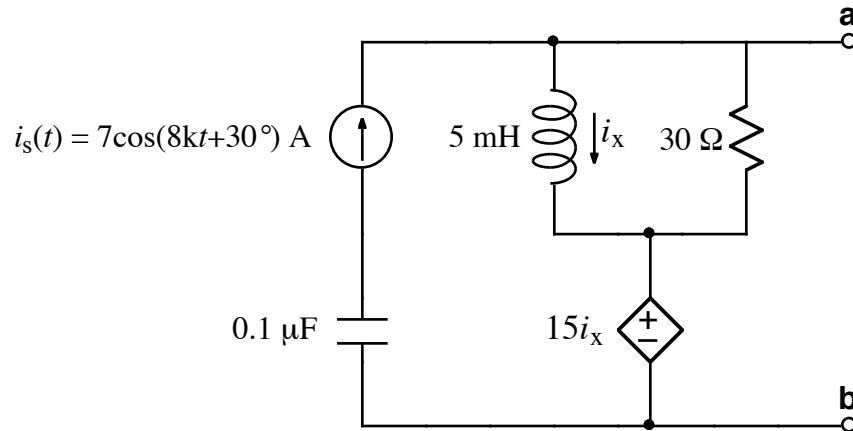


Ex:



- Draw a frequency-domain equivalent of the above circuit. Show a numerical phasor value for $i_s(t)$, and show numerical impedance values for R, L, and C. Label the dependent source appropriately.
- Find the Thevenin equivalent (in the frequency domain) for the above circuit. Give the numerical phasor value for V_{Th} and the numerical rectangular form for the impedance value of z_{Th} .

sol'n: a) We compute phasors and impedances.

$$P[i_s(t)] = P[7\cos(8kt + 30^\circ)A]$$

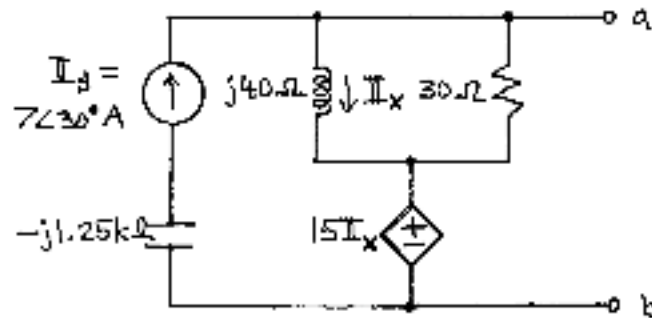
$$\text{or } I_s = 7\angle 30^\circ A$$

$$\frac{-j}{\omega C} = \frac{-j}{8k \cdot 0.1\mu} = -j \frac{1k\Omega}{0.8} = -j 1.25k\Omega$$

$$j\omega L = j 8k \cdot 5m \Omega = j 40\Omega$$

$$I_x = P[i_x]$$

Frequency- or s-domain model:



- b) The $-j1.2 \text{ k}\Omega$ is in series with a current source and may be ignored.

Also, with no load connected across **a** and **b**, (the condition under which we measure V_{Th} across **a** and **b**), the $j40 \Omega$ and 30Ω form a current divider.

$$\begin{aligned} I_x &= I_s \cdot \frac{30 \Omega}{30 \Omega + j40 \Omega} \\ &= 7\angle 30^\circ \text{ A} \cdot \frac{30}{30 + j40} \\ &= 7\angle 30^\circ \text{ A} \cdot \frac{30}{50\angle 53.1^\circ} \\ &= \frac{21}{5} \angle 30^\circ - 53.1^\circ \\ &= \frac{21}{5} \angle -23.1^\circ \end{aligned}$$

To obtain an exact expression for I_x , we may use the following alternative calculation:

$$I_x = I_s \cdot \frac{30\Omega}{30\Omega + j40\Omega}$$

$$\text{where } I_s = 7 \angle 30^\circ \text{ A} = 7 \frac{\sqrt{3}}{2} + j \frac{7}{2}$$

$$I_x = 7 \cdot \left(\frac{\sqrt{3}}{2} + j \frac{1}{2} \right) \cdot \frac{30\Omega}{30\Omega + j40\Omega} = \frac{30\Omega - j40\Omega}{30\Omega - j40\Omega} \text{ A}$$

$$= \frac{\frac{21}{2} (\sqrt{3} + j1)}{3^2 + 4^2} \text{ A}$$

$$= \frac{21}{25} \cdot \frac{1}{2} (3\sqrt{3} + 4 - j4\sqrt{3} + j3) \text{ A}$$

$$I_x = \frac{21}{50} [3\sqrt{3} + 4 + j(3 - j4\sqrt{3})] \text{ A}$$

Now we have $V_{Th} = V_{ab}$:

$$V_{Th} = 15 I_x + I_s j40\Omega \parallel 30\Omega$$

$$\text{or } V_{Th} = 15 I_x + j40\Omega I_x$$

$$= (15 + j40\Omega) \frac{21}{50} [3\sqrt{3} + 4 + j(3 - j4\sqrt{3})] \text{ V}$$

$$= \frac{21}{50} (45\sqrt{3} + 60 - 120 + 160\sqrt{3} + j45 - j60\sqrt{3} + j120\sqrt{3} + j160) \text{ V}$$

$$V_{Th} = \frac{21}{50} \left[205\sqrt{3} - 60 + j(60\sqrt{3} + 205) \right] V$$

$$V_{Th} = \frac{21}{10} \left[41\sqrt{3} - 12 + j(12\sqrt{3} + 41) \right] \doteq 21\sqrt{73} \angle 46.3^\circ V$$

If we opt for an approximate answer, we have the following result:

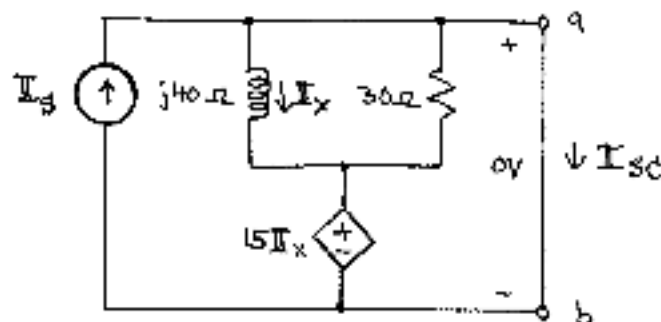
$$V_{Th} = (15 + j40 \Omega) I_x$$

$$\doteq 5(3 + j8) \cdot \frac{21}{5} \angle -23.1^\circ V$$

$$= 21 \cdot \sqrt{73} \angle 69.4^\circ - 23.1^\circ V$$

$$V_{Th} = 21\sqrt{73} \angle 46.3^\circ V$$

Now we find Z_{Th} using $Z_{Th} = \frac{V_{Th}}{I_{sc}}$.



We observe that shorting **a** to **b** gives 0V across the components in the middle. We suspect all of I_s flows in the wire from **a** to **b**, meaning $I_x = 0$ and $15I_x = 0V$.

We check whether $I_x = 0$ and $15I_x = 0V$ is plausible. It does because if $15I_x = 0V$, then we have $0V - 0V = 0V$ across the $j40\Omega$ and 30Ω . Thus, $I_x = \frac{0V}{j40\Omega} = 0$.

So $I_x = 0$ is consistent, and $I_{sc} = I_g$.

$$\therefore Z_{Th} = \frac{V_{Th}}{I_{sc}} = \frac{V_{Th}}{I_g}$$

$$\doteq \frac{21\sqrt{73} \angle 46.3^\circ V}{7 \angle 30^\circ A}$$

$$\doteq 3\sqrt{73} \angle 46.3^\circ - 30^\circ \Omega$$

$$Z_{Th} \doteq 3\sqrt{73} \angle 16.3^\circ \Omega$$

