

Find  $v_o(t)$ . No energy stored in circuit at  $t=0$ .

$$\text{ans: } v_o(t) = [-45t e^{-5t} + 24e^{-5t}] u(t) \text{ V}$$

sol'n: We apply the general procedure for solving circuit problems in the Laplace domain:

- 1) Laplace transform each current or voltage source.

$$\text{Here, } \mathcal{L}\{i_g(t)\} = 15u(t)A \Rightarrow 15 \cdot \frac{1}{s} A = I_g(s).$$

The dependent source becomes

$$\mathcal{L}\{0.4V_\phi(t)\} = 0.4V_\phi(s) \text{ where } V_\phi(s) = \mathcal{L}\{v_\phi(t)\}$$

Note: It is still a dependent source in the s-domain. It depends on Laplace transformed voltage,  $V_\phi(s)$ . (We must determine  $V_\phi(s)$  at some point below.)

- 2) Laplace transform each circuit element R, L, or C.

Note: If initial conditions are nonzero for L or C, we may choose whichever of two possible s-domain equivalents is most convenient.

$$\mathcal{L}\left\{\frac{1}{R}R\right\} = \frac{1}{R} \quad \text{No change.}$$

$$v(t) = R i(t)$$

Note: R's are not freq. sensitive  $\Rightarrow$  same in t- and s-domains.

$$V(s) = R I(s)$$

$$\begin{aligned}
 L \left\{ i_L(t) \right\} &= + \quad \text{at } t=0^- \\
 &= V_L(s) - L i_0 \\
 &= V(s) - \frac{1}{s} i_0 \\
 &= V(s) - \frac{1}{s} L \left\{ i_L(t) \right\}
 \end{aligned}$$

initial current  
 at  $t=0^-$

Note: The sources in the *s*-domain represent signals that create the initial conditions for the *L*. In the first case, the *t*-domain equivalent of *V*-source  $-L i_0$  is  $-L i_0 \delta(t)$ . This means that a delta function voltage in series with an *L* will leave the *L* with a current of  $i_L(t=0^+) = i_0$ . In the second case, the *t*-domain equivalent of *I*-source  $i_0/s$  is  $i_0 u(t)$ . This means that we simply turn on a current source at  $t=0$  to carry the initial current on the *L*. This current source is considered to be inside the *L*, but we end up treating it like just another circuit element. It is somewhat remarkable that we can handle initial conditions by adding a source that we may treat mathematically as distinct from the *L*.

Another subtlety is that our *s*-domain models have zero initial conditions at time  $t=0^-$  and become equivalent to the *t*-domain component at time  $t=0^+$  owing to events (such as step or delta functions) occurring at  $t=0$ . This practice allows us to use superposition when handling initial conditions, (i.e. we just add some sources to our zero-initial-condition circuit).

$$\mathcal{L} \left\{ v_o + \frac{1}{sC} \right\} = \frac{1}{sC} V_c(s) = \frac{1}{sC} = \frac{1}{sC} + \frac{V_c(s)}{sC} = \frac{1}{sC} + \frac{CV_o}{sC}$$

$\mathcal{L} \{ v_o u(t) \}$

*initial voltage  $v_o$*

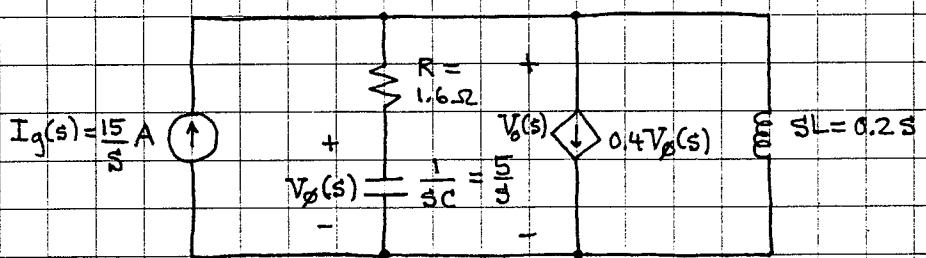
$\mathcal{L} \{ C v_o s(t) \}$

Note: The  $V$ -source in the first of the above two s-domain models creates the initial voltage on the  $C$  by adding a voltage that steps to  $v_o$  at time  $t=0$ .

The  $I$ -source in the second of the above two s-domain models creates the initial voltage on the  $C$  by injecting an appropriate amount of charge on the  $C$  via a delta-function current source. The current is infinite for zero duration and delivers a finite charge, (just as the  $S(t)$  is infinite for zero duration and has a finite area). The voltage we are left with is  $v_o = \frac{1}{C} \int_{0^-}^{0^+} i_C(t) dt = \frac{1}{C} \int_{0^-}^{0^+} C v_o s(t) dt$

$$= C v_o \int_{0^-}^{0^+} s(t) dt = C v_o \cdot 1 = v_o$$

Since initial conditions are zero for problem 13.11, our initial condition sources disappear, leaving us with the following s-domain model:



- 3) In general, we now apply superposition to find  $V_o(s)$  as the sum of  $V_{oi}(s)$  values for one independent source at at time turned on.

Here, we have only one independent source.

Note: Initial conditions on L's and C's are created by sources that we treat as independent sources. Thus, we effectively turn on one initial condition at a time — or we solve for one input signal (independent source) with initial conditions equal zero — when we apply superposition.

- 4) Solve the circuit use node-V or mesh-I methods.

Here, we use node-V method:

$$\text{constraint eq'n: } V_o(s) = V_o(s) \cdot \frac{1/sC}{1/sC + R} \quad \text{V-divider}$$

$$\text{node-V (sum of currents = 0): } -\frac{15}{s} + \frac{V_o(s)}{1+R} + \frac{0.4V_o(s)}{sL} + \frac{V_o(s)}{sC} = 0A$$

$$\text{or } V_o(s) \left[ \frac{1}{1+R} + \frac{0.4}{1+R} \frac{1/sC}{sC} + \frac{1}{sL} \right] = \frac{15}{s}$$

$$\text{or } V_o(s) \left[ \frac{1}{1+R} + \frac{0.4sL}{sC} + \frac{1}{sC} \right] = \frac{15}{s} \frac{sL(1+R)}{sC}$$

$$\text{or } V_o(s) \left[ \frac{s^2LC}{sC} + \frac{0.4sL}{sC} + \frac{1}{sC} \right] = 15L(1+sRC)$$

We need a coefficient = 1 for highest-order s term.

$$\text{or } V_o(s) \left[ s^2 + \frac{0.4s}{C} + \frac{1}{LC} + s \frac{R}{L} \right] = \frac{15R}{C} \left( 1 + \frac{SRC}{RC} \right)$$

$$\text{or } V_o(s) = 15R \left( s + \frac{1}{RC} \right)$$

$$s^2 + \left( \frac{0.4}{C} + \frac{R}{L} \right) s + \frac{1}{LC}$$

$$\frac{1}{RC} = \frac{1}{1.6 \cdot 0.2} = \frac{5}{1.6} \quad \frac{0.4}{C} = 5 (0.4) = 2$$

$$\frac{R}{L} = \frac{1.6}{0.2} = 8 \quad \frac{1}{LC} = \frac{1}{(0.2)(0.2)} = 25$$

$$15R = 15 \cdot 1.6 = 24$$

$$\therefore V_o(s) = \frac{24 (s + 5/1.6)}{s^2 + 10s + 25} = \frac{24s + 75}{(s+5)^2}$$

5) Use partial fraction expansion in s-domain.

$$V_o(s) = \frac{K_1}{(s+5)^2} + \frac{K_2}{s+1}$$

$$\text{where } K_1 = V_o(s) \Big|_{s=5}^2$$

$$K_2 = \frac{d[V_o(s)(s+5)]}{ds} \Big|_{s=-5}$$

$$K_1 = 24s + 75 \Big|_{s=-5} = -45$$

$$K_2 = \frac{d(24s + 75)}{ds} \Big|_{s=-5} = 24 \Big|_{s=-5} = 24$$

Note: The general formula for  $K_m$  with a root repeated  $n$  times is:

$$K_m = \frac{1}{(m-1)!} \frac{d^{m-1}}{ds^{m-1}} [F(s) \cdot (s+a)^n]$$

The  $\frac{1}{(m-1)!}$  only comes into play when  $m \geq 3$ .

6) Use inverse Laplace Transform formula

$$\mathcal{L}^{-1} \left\{ \frac{1}{(s+a)^n} \right\} = \frac{t^{n-1} e^{-at}}{(n-1)!} u(t)$$

Note: The  $\frac{1}{(n-1)!}$  only comes into play when  $n \geq 3$ .

Here, we get  $v_o(t) = [-45t e^{-5t} + 24 e^{-5t}] u(t)$

$$v_o(t) = [-45t + 24] e^{-5t} u(t).$$