

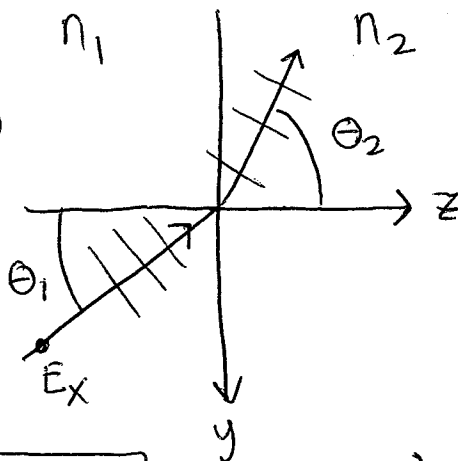
Wave description of TIR

$$E_1 = \hat{x} E_0 e^{-jk_0 n_1 (z \cos \theta_1 - y \sin \theta_1)}$$

$$E_2 = \tau \hat{x} E_0 e^{-jk_0 n_2 (z \cos \theta_2 - y \sin \theta_2)}$$

$$\sin \theta_2 = \frac{n_1}{n_2} \sin \theta_1$$

$$\cos \theta_2 = \sqrt{1 - \frac{n_1^2}{n_2^2} \sin^2 \theta_1}$$



$$E_2 = \tau \hat{x} E_0 e^{-jk_0 n_2 \left(z \sqrt{1 - \frac{n_1^2}{n_2^2} \sin^2 \theta_1} - y \frac{n_1}{n_2} \sin \theta_1 \right)}$$

wave fronts in-phase at interface, i.e. tangential components continuous

$$(n_2 \sin \theta_2 = n_1 \sin \theta_1)$$

phase velocity @ interface

$$y k_0 n_1 \sin \theta_1 + \omega t = \text{const}$$

$$\Rightarrow \frac{dy}{dt} = v_{\text{node}} = -\frac{\omega}{k_0 n_1 \sin \theta_1} = \frac{v_{\text{phase 1}}}{\sin \theta_1} \quad (= \frac{v_{\text{phase 2}}}{\sin \theta_2})$$

$$v_{\text{phase 1}} = c/n_1$$

at $\theta_1 = \theta_{cr}$, $\cos \theta_2 \rightarrow 0$ $\sin \theta_2 \rightarrow 1$

$$E_2 = \tau \hat{x} e^{jk_0 n_2 y}$$

plane wave travelling || to interface along y-dir

$$v_{\text{node}} = v_{\text{phase 2}} = \text{mm. velocity}$$

for $\theta_1 > \theta_{cr}$ $\sqrt{\quad}$ becomes imaginary

$$E_2 = \tau \hat{x} E_0 e^{-k_0 n_2 \sqrt{(n_1/n_2)^2 \sin^2 \theta_1 - 1} z} e^{jk_0 n_1 \sin \theta_1 y}$$

$$= \tau \hat{x} E_0 e^{-\gamma z} e^{j\beta y}$$

$$\gamma = \text{attenuation coefficient (cm}^{-1}\text{)} = k_0 n_2 \sqrt{\frac{n_1^2}{n_2^2} \sin^2 \theta_1 - 1}$$

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②

$\beta = k_0 n_1 \sin \theta_1$ propagation coefficient (rad/cm)

E_z decays exponentially along z and is known as evanescent

E and H are 90° out of phase, reactive power where energy is stored, but no work done

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} = -\mu_0 \frac{\partial \vec{H}}{\partial t}$$

$$\begin{aligned} \nabla \times \vec{E} &= \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ E_2 & 0 & 0 \end{vmatrix} = \hat{y} \frac{\partial E_2}{\partial z} - \hat{z} \frac{\partial E_2}{\partial y} \\ &= -j\omega \hat{y} E_2 - j\beta \hat{z} E_2 \\ &= -j\omega \vec{B} = -j\omega \mu_0 \vec{H} \end{aligned}$$

$$\vec{H} = \underbrace{\frac{j}{\omega \mu_0} E_2}_{90^\circ \text{ phase}} \hat{y} + \frac{\beta}{\omega \mu_0} E_2 \hat{z}$$

look @ power $S_z = \frac{1}{2} \text{Re} [\vec{E} \times \vec{H}^* \cdot \hat{z}]$

$$\begin{aligned} \vec{E} \times \vec{H}^* &= \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ E_2 & 0 & 0 \\ 0 & -\frac{j}{\omega \mu_0} E_2^* & \frac{\beta}{\omega \mu_0} E_2^* \end{vmatrix} = \hat{z} \cdot \frac{j}{\omega \mu_0} |E_2|^2 \\ &\quad - \hat{y} \frac{\beta}{\omega \mu_0} |E_2|^2 \end{aligned}$$

$$S_z = \frac{1}{2} \text{Re} \left[\frac{j}{\omega \mu_0} |E_2|^2 \right] = \underline{\underline{0}}$$

Phase shift upon reflection

upon TIR, phase of reflection lags incident

⇒ extra distance light travels into and from low index medium known as Goos-Hänchen shift

$$\frac{E_r}{E_i} = \frac{n_1 \cos \theta_1 - n_2 \cos \theta_2}{n_1 \cos \theta_1 + n_2 \cos \theta_2} = |r| e^{j2\phi}$$

$$= \frac{\alpha - j\beta}{\alpha + j\beta} \quad \alpha = n_1 \cos \theta_1$$

$$j\beta = n_2 \cos \theta_2$$

$$2\phi_{TE} = 2 \tan^{-1} \left(\frac{-\sqrt{n_1^2 \sin^2 \theta_1 - n_2^2}}{n_1 \cos \theta_1} \right) \quad \theta_1 > \theta_{cr}$$

$$|E_r/E_i| = 1$$

$$2\phi_{TM} = 2 \tan^{-1} \left(-\frac{n_1^2}{n_2^2} \frac{\sqrt{n_1^2 \sin^2 \theta_1 - n_2^2}}{n_1 \cos \theta_1} \right)$$

Goos-Hänchen shift (Appendix A)

need to have beam, two incident plane waves

$$\beta \pm \Delta\beta$$

$$A(z) = [e^{j\Delta\beta z} + e^{-j\Delta\beta z}] e^{-j\beta z}$$

$$= 2 \cos(\Delta\beta z) e^{-j\beta z} \quad @ \quad x=0$$

for small $\Delta\beta$, $\phi(\beta \pm \Delta\beta) = \phi(\beta) + \frac{\partial \phi}{\partial \beta} \Delta\beta$

$$B(z) = 2 \cos \Delta\beta (z - z_s) e^{-j\beta z} \quad z_s = d\phi/d\beta$$

for TE, $k_0 z_s = \tan \theta / \sqrt{\beta^2 - n_2^2}$ Goos-Hänchen shift

$$x = z_s / \tan \theta = 1/\gamma \quad \text{attenuation length}$$

