

ECE 5130/6130 Final Exam

May 2, 2001

Name Key

You may use your portfolio, lab notebook and calculator. No textbooks.

PLEASE TURN YOUR PORTFOLIO AND LAB BOOK INTO THE ECE OFFICE (BOX NEXT TO AMBER).

Time: 1 hour and 50 minutes

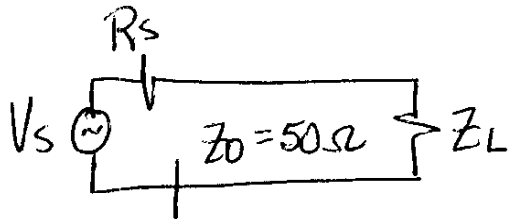
Part I (can be used to replace Midterm I)	=	Problems 1 and 2
Part II (can be used to replace Midterm II)	=	Problems 3 and 4
Part III (all students must complete)	=	Problems 5 and 6

Good Luck! Do well.

1. Steady-state transmission lines: (30 points)

A 50 ohm transmission line 5.2 meters long is connected to a 25 ohm generator. The voltage loss term,  $\alpha$ , is 0.1 nepers / meter. The wavelength is 1 meter. The input impedance is measured to be 35 ohms. What is the load impedance?

$$Z_L = 85 - j67.5 \text{ ohms}$$



$$Z_{in} = 35 + j0 \Omega$$

Normalize & Plot:

$$Z_{in}(n) = \frac{Z_{in}}{Z_0} = 0.7 + j0$$

Compute loss

$$e^{-2\alpha z} = e^{-2(0.1 \text{ Np/m})(5.2 \text{ m})} = 0.35$$

Not accounting for loss  
-10

Rotate  $Z_{in}$   $5.2\lambda$   $TWL$  ( $= 0.2\lambda$   $TWL$ ) to  $Z_L(n)$

$$\text{Read } |\Gamma_a| = 0.18 \quad -5$$

Find  $|\Gamma_{Load}|$ , considering loss:

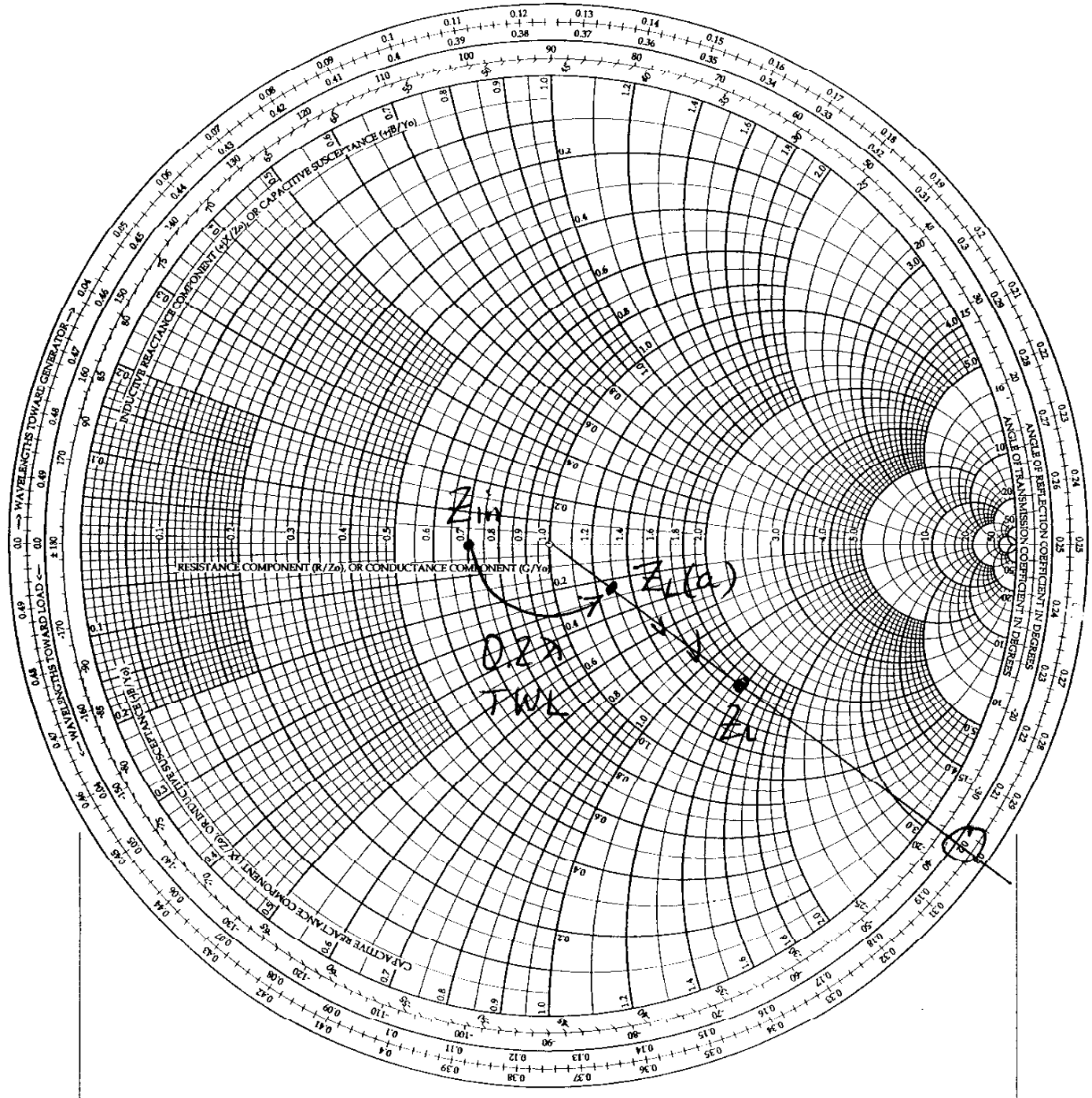
$$|\Gamma_{Load}| = \frac{|\Gamma_a|}{e^{-2\alpha z}} = \frac{0.18}{0.35} = 0.51 \quad \text{Plot } Z_L$$

$$\text{Read } Z_L = 1.7 - j1.35$$

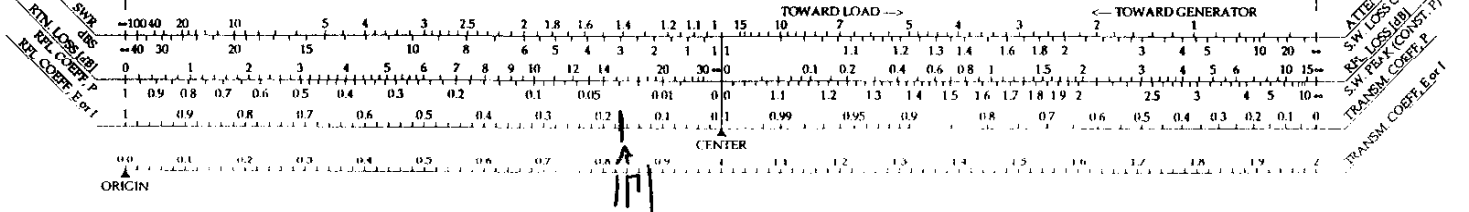
$$\text{Denormalize } Z_L(n) = (1.7 - j1.35) 50 \Omega = 85 - j67.5 \Omega$$

# The Complete Smith Chart

## Black Magic Design



### RADIALLY SCALED PARAMETERS



## 2. Impedance Matching

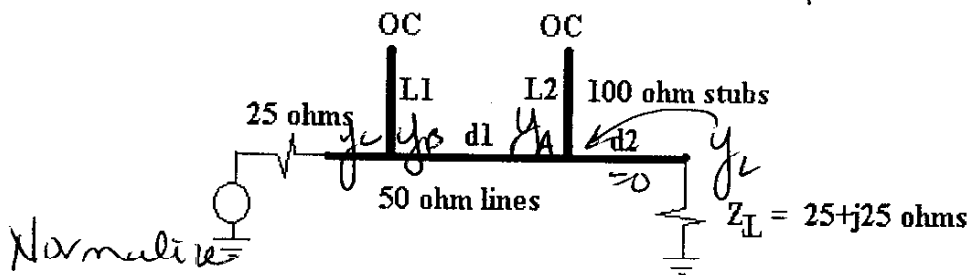
Design a double stub matching network. The load impedance is  $25 + j25$  ohms. The generator impedance is  $25$  ohms. The characteristic impedance of all of the lines is  $50$  ohms. The characteristic impedance of the stubs is  $100$  ohms, and they are terminated by open circuits.

$$d_2 = 0 \text{ wavelengths}$$

$$L_1 = 0 \parallel 0.24 \text{ wavelengths}$$

$$d_1 = 0.125 \text{ wavelengths}$$

$$L_2 = 0.176 \parallel 0.224 \text{ wavelengths}$$



Normalize

$$Z_L = \frac{25 + j25}{50} = \frac{1}{2} + j\frac{1}{2}$$

Plot, Reflect thru origin to  $y_L = 1 - j1$

Draw matching circle rotated  $.125\lambda$  TWT

Move  $y_L$  along constant real circle to rotated matching circle to  $y_{A1}$  or  $y_{A2} = y_{\text{stub } 2} + y_L$

$$\text{Read } y_{A1} = 1 + j0$$

$$y_{A2} = 1 + j2.0$$

$$\text{Calc. } y_{s2_1} = y_{A1} - y_L = (1 + j0) - (1 - j1) = j1 \quad y_{s2_2} = (1 + j2) - (1 - j1) = j3$$

Denormalize to  $50\Omega$  & Renormalize to  $100\Omega$ . Plot, Rotate TWT to  $y_{oc}$

$$y_{s2_1} = (j1) \left( \frac{1}{50\Omega} \right) \left( \frac{1}{100\Omega} \right) = j2$$

$$y_{s2_2} = (j3) \left( \frac{1}{50\Omega} \right) = j6$$

Plot & Rotate  $.125\lambda$  TWT Back to regular matching  $100\Omega$  circle. Read

$$y_{B1} = 1 + j0$$

$$y_{B2} = 1 - j2$$

$$\text{Want } y_c = 1 + j0 = y_{\text{stub } 1} + y_B$$

$$y_{\text{stub } 1} = 0 + j$$

$$y_{\text{stub } 2} = +j2$$

Denormalize ( $50\Omega$ ); Renormalize ( $100\Omega$ ); Plot

$$y_{\text{stub } 1} = 0 \frac{1/50}{1/100} = j0$$

$$y_{\text{stub } 2} = (j2) \frac{1/50}{1/100} = j4$$

Rotate TWT to  $y_{oc}$

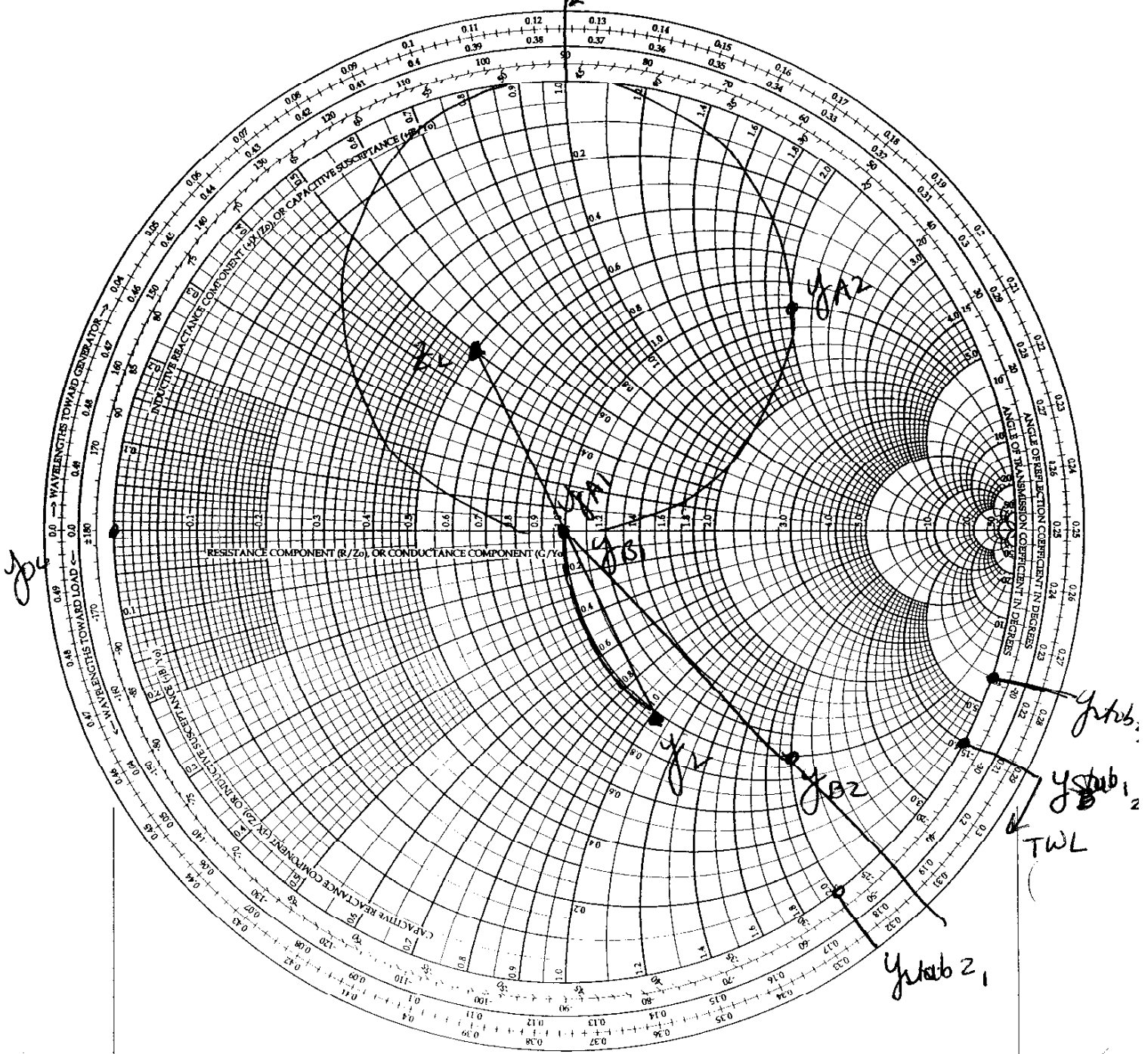
$$L_1 = 0$$

$$L_2 = 0.24\lambda$$

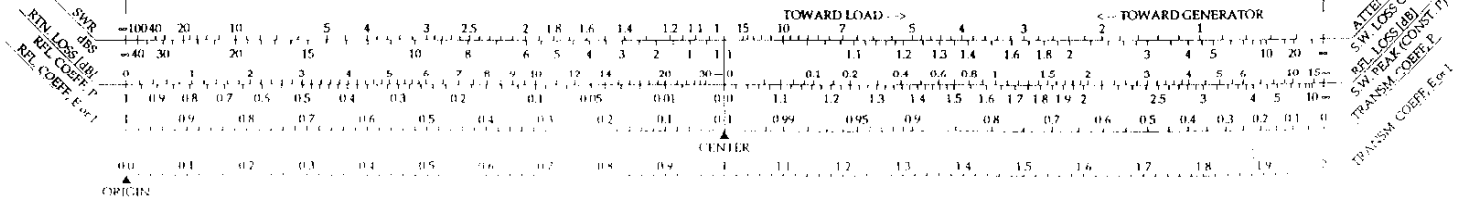
# The Complete Smith Chart

Black Magic Design

← .125 λ TL



RADIALLY SCALED PARAMETERS



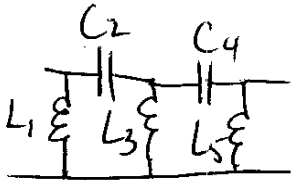
ATTEN (dB)  
SW LOSS COEFF  
SW PEAK COEFF (V)  
TRANSM. COEFF. E (V)

### 3. Filters

- (a) Design a maximally flat high pass filter with a cutoff frequency of 3 GHz, impedance of 50 ohms, and at least 15 dB of insertion loss at 2 GHz. Sketch the filter and specify the L,C components that will be used for a lumped element filter.
- (b) Design a stepped impedance filter for a low pass design with cutoff at 2 GHz and at least 15 dB of insertion loss at 3 GHz. (Note that this can be done by converting the values you obtained in part a above.) Match your filter to a 50 ohm line. The minimum impedance that can be used is 10 ohms, and the maximum is 100 ohms.
- (c) Sketch your design, and clearly specify the lengths and impedances of all lines.

(a)  $\left| \frac{\omega_c}{\omega} \right| - 1 = \left| \frac{3}{2} \right| - 1 = 0.5 \Rightarrow \text{Fig 8.26 p450 } \boxed{N=5}$

Table 8.3:  $g_1 = 0.6180 \quad g_2 = 1.6180 \quad g_3 = 2.0$   
 $g_4 = 1.6180 \quad g_5 = 0.6180 \quad g_6 = 1.0$

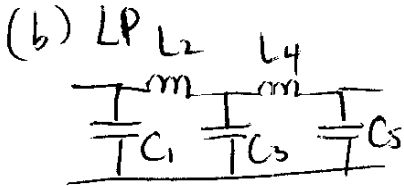


$$L_1 = \frac{R_0}{\omega_c g_1} = \frac{50}{(2\pi \cdot 3e9)(0.6180)} = 4.29 \text{ nH}$$

$$C_2 = \frac{1}{R_0 \omega_c g_2} = \frac{1}{(50)(2\pi \cdot 3e9)(1.6180)} = .656 \text{ pF}$$

$$L_3 = \frac{50}{(2\pi \cdot 3e9)(2.0)} = 1.33 \text{ nH}$$

$$C_4 = C_2 \quad L_5 = L_1$$



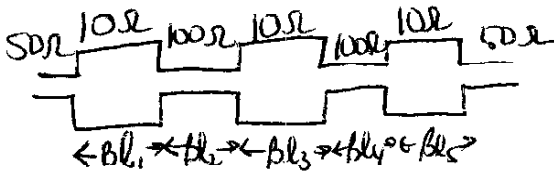
$$Bl_1 = \frac{g_1 Z_L}{R_0} = \frac{(0.6180)(10)}{50} = .1236$$

$$Bl_2 = \frac{g_2 Z_0}{Z_h} = \frac{(1.6180) \frac{50}{100}}{50} = .809$$

$$Bl_3 = \frac{g_3 Z_L}{R_0} = \frac{(2.0)(10)}{50} = 0.4$$

$$Bl_4 = Bl_2$$

$$Bl_5 = Bl_1$$



$$Z_L = 10\Omega \quad Z_h = 100\Omega$$

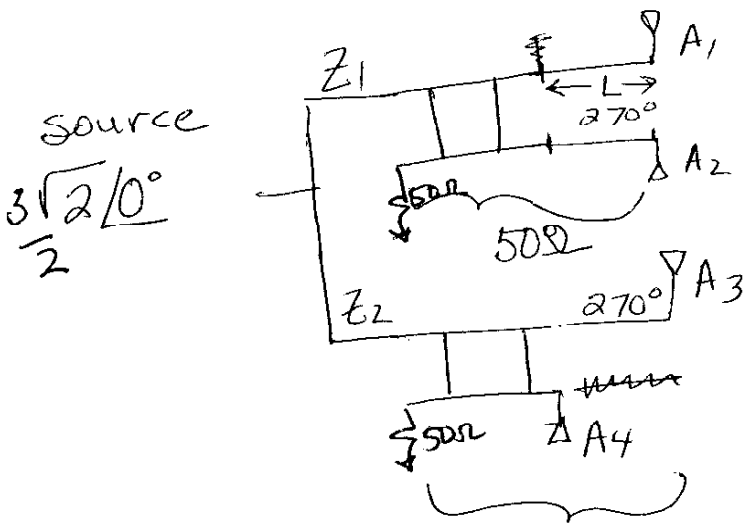
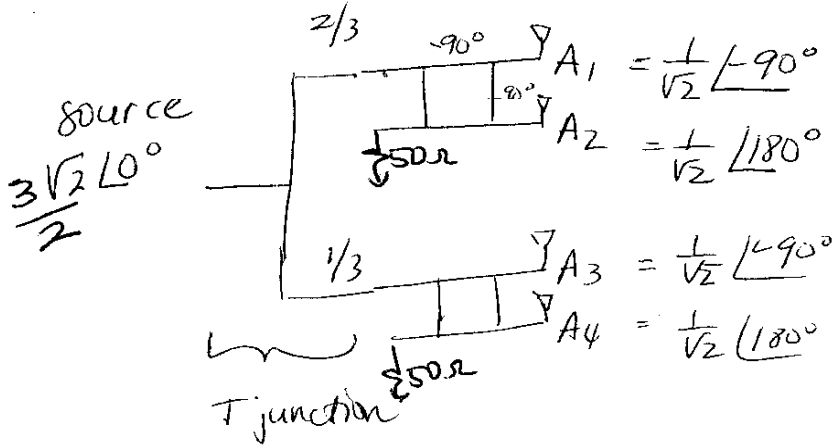
#### 4. Power Dividers

Design a power divider to feed four antennas with the following magnitudes, phases, and characteristic impedances:

- Antenna 1:  $1.0 \angle 0^\circ$  volts      50 ohms
- Antenna 2:  $1.0 \angle -90^\circ$  volts      50 ohms
- Antenna 3:  $0.5 \angle 0^\circ$  volts      100 ohms
- Antenna 4:  $0.5 \angle 180^\circ$  volts      100 ohms

*There are many ways to solve this problem...*

You may use any combination of the power dividers we have studied, lossless transmission lines, matching networks, etc. Sketch your system and clearly label all parts of the network, the location where each antenna is connected, and what the input voltage should be.



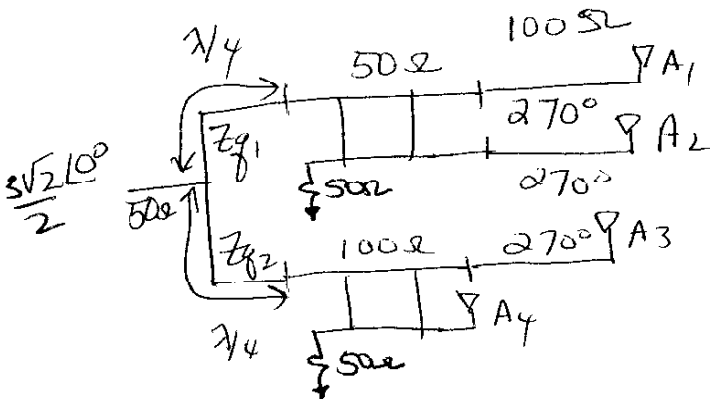
$$Z_1 = \frac{3}{2} Z_0 = 75 \Omega$$

$$Z_2 = 3 Z_0 = 150 \Omega$$

Design Qwave TX between  $Z_1, Z_2$  & Qcouplers

$$Z_{q1} = \sqrt{Z_1 50 \Omega} =$$

$$Z_{q2} = \sqrt{Z_2 100 \Omega} =$$



### 5. Rectangular Waveguides

An X-band waveguide has a recommended frequency range of 8.20-12.4 GHz. This WR-90 waveguide has inside dimensions of 2.286x1.016 cm.

- What are the first three waveguide modes and their cutoff frequencies?
- Why is the recommended frequency range of this waveguide given as 8.20-12.4 GHz?
- Assume the wave is propagating in the z-direction. Write an equation for  $E_x$  if all of the first three modes are propagating.

$$(a) f_c = \frac{c_0}{2\pi \sqrt{\mu_r \epsilon_r}} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2}$$

$$TE_{10} f_c = \frac{c_0}{2\pi} \sqrt{\left(\frac{\pi}{2.286e-2}\right)^2} = 6.56 \text{ GHz}$$

$$TE_{20} f_c = \frac{c_0}{2\pi} \sqrt{\left(\frac{2\pi}{2.286e-2}\right)^2} = 13.12 \text{ GHz}$$

$$TE_{01} f_c = \frac{c_0}{2\pi} \sqrt{\left(\frac{\pi}{1.016e-2}\right)^2} = 14.76 \text{ GHz}$$

$$TE_{11} f_c = \frac{c_0}{2\pi} \sqrt{\left(\frac{\pi}{2.286e-2}\right)^2 + \left(\frac{\pi}{1.016e-2}\right)^2} = 16.16 \text{ GHz}$$

First 3 modes

(b) This is slightly higher than the cutoff for first mode, which ensures it will propagate. It is slightly lower than the second mode, ensuring that it will not propagate.

$$(c) E_x = \frac{j\omega\mu n\pi}{k_c^2 b} A_{mn} \cos \frac{m\pi x}{a} \sin \frac{n\pi y}{b} e^{-j\beta z}$$

$$A_{mn} = \frac{j\omega\mu A}{k_c^2}$$

$$k_c = \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2}$$

$$\beta = \sqrt{k^2 - k_0^2}$$

$$k = \omega\sqrt{\mu\epsilon}$$

Sum 3 modes

$$E_x = \underbrace{\frac{j\omega\mu(0)\pi}{k_{c10}^2 b}}_{TE_{10}} + \underbrace{\frac{j\omega\mu(0)\pi}{k_{c20}^2 b}}_{TE_{20}} + \frac{j\omega\mu(1)}{k_{c01}^2 b} \cos 0 \sin \frac{\pi y}{b} e^{-j\beta z}$$

$\uparrow = \pi/b$



## 6. Circular Waveguide

A circular waveguide is filled with sea water  $\epsilon_r = 80.0$  and  $\sigma = 0.1$  S/m (ignore changes in the electrical properties as a function of frequency). The radius of the waveguide is 3 cm.

- (a) Write the equation you will use to find the cutoff frequency of the modes in the waveguide.
- (b) What is the first mode of the waveguide and its cutoff frequency?
- (c) In the derivation of the modes of a circular waveguide, we were able to eliminate the  $Y_n(\cdot)$  term. Why?
- (d) Describe what would happen to a pulse with an "infinite" bandwidth in this waveguide. Tell what will happen to ALL of the power in the pulse (for any power that is not transmitted, tell where it goes). Explain what causes any changes to the shape of the pulse as it transmits through the waveguide.

$$(a) f_c = \frac{k_c v_p}{2\pi} = \frac{p_{nm} c_0}{2\pi a} =$$

(b) TE<sub>11</sub> (first mode)

$$f_c = \frac{p'_{11} c_0}{2\pi a} = \frac{(1.8) 3e8 \text{ m/s}}{2\pi (0.03)} =$$

(c)  $y_n(x) = -\infty$  @  $x=0$  (center of waveguide)  
Nonphysical sol<sup>n</sup> can be removed

- (d)
- ① Freqs below cutoff will be made into evanescent waves & won't propagate
  - ② Propagating modes each have different  $v_p$ , resulting in ~~alternating~~ dispersion
  - ③ All fields will attenuate, each mode/freq. @ a different rate

ECE 5130/6130 Final Exam

Problem 1 \_\_\_\_\_ / 30

Problem 2 \_\_\_\_\_ / 30

Total of 1&2 \_\_\_\_\_ / 60

Problem 3 \_\_\_\_\_ / 30

Problem 4 \_\_\_\_\_ / 30

Total of 3&4 \_\_\_\_\_ / 60

Problem 5 \_\_\_\_\_ / 30

Problem 6 \_\_\_\_\_ / 30

Total of 5&6 \_\_\_\_\_ / 60

Total \_\_\_\_\_ / 180