

## ECE 540 Final Exam –Take Home

Winter Quarter, 1998

Name: Key

Date: \_\_\_\_\_

Time picked up: 8

Time returned: \_\_\_\_\_

You may use any books, notes, computer, calculator, etc. Show complete solutions including your work. PLEASE do NOT consult with any person (other students, instructors, etc.) about this exam.

1. Design a single stub tuner to match an antenna with  $Z_L = 25 + j25\Omega$  to a  $50\Omega$  microstripline.

Specify: Parallel or series stub \_\_\_\_\_

Open or short circuit stub \_\_\_\_\_

Justify your choice of the type of tuner you choose.

Distance from load to stub  $d = \cancel{0.0433\lambda} \quad 0.0738\lambda$

Length of stub  $L = \cancel{0.0898\lambda} \quad 0.125\lambda$

~~$$Z_{Ln} = \frac{Z_L}{Z_0} = \frac{25 + j50}{50} = \frac{1}{2} + j1$$~~

~~Using TLine software~~

~~Rotate TWTG  $0.0433\lambda = d$  to matching circle~~

~~Read  $Z_{Lsn} = 1 + j1.58$~~

~~Stub needs to have  $Z_s = -j1.58$~~

~~Plot on Smith Chart~~

~~Rotate TWTL  $0.0898\lambda = L$~~

parallel open

$d = 0\lambda$   
or  $0.5\lambda$

$l = 0.125\lambda$

$$Z_{Ln} = \frac{Z_L}{Z_0} = \frac{25 + j25}{50} = \frac{1}{2} + j\frac{1}{2}$$

Plot on Smith Chart (I used TLine software)

Rotate TWTG  $0.0738\lambda = d$  to matching circle

Read  $Z_n = 1 + j$

Stub needs to have  $Z_s =$

Plot on smith chart, Rotate TWTL to  $Z_{open}$ .

$L = 0.125\lambda$

2. Design a double stub tuner to match the same antenna to a  $50 \Omega$  co-axial line.

Distance from load to first stub =  $0.1\lambda$

Distance between stubs =  $0.3\lambda$

Specify: Parallel or series stub \_\_\_\_\_

Open or short circuit stub \_\_\_\_\_

Justify your choice of tuner.

Length of first stub (nearest load) \_\_\_\_\_

Length of second stub (nearest source) \_\_\_\_\_

Plot  $Z_{in} = \frac{1}{2} + j\frac{1}{2}$ . Convert to admittance.

Rotate  $0.1\lambda$  TWG

Rotate matching circle  $0.3\lambda$  TWG

Move along constant R circle to <sup>rotated</sup> matching circle

Option 1

Length of Stub 1 =  $0.173\lambda$   
 ~~$0.523\lambda$~~

2 =  $0.0905\lambda$

Option 2

$L1 = 0.331\lambda$

$L2 = 0.366\lambda$

Series Short

$L1 = \text{No Soln}$        $L1 =$

$L2 =$                        $L2 =$

3.

(a) Choose a circular waveguide (see attached table) for use transmitting a signal at 9GHz.

WC109  
WC94

$$f_{cmn} = \frac{P'_{nm}(c)}{2\pi a \sqrt{\epsilon_r}}$$

TE

$$TM = \frac{P'_{nm}(c)}{2\pi a \sqrt{\epsilon_r}}$$

Er = 1.0 air  
C = 2.996e8 m/s

a = inner radius =  $\frac{1.094''}{2}$   
a = 0.013894m

(b) Specify the first four modes of this waveguide and their frequencies.

P<sub>01</sub> = 2.405    P'<sub>01</sub> = 3.832    TE<sub>11</sub>    f<sub>c11</sub> = ~~6.32~~ 6.32 GHz  
 P'<sub>11</sub> = 1.841    TM<sub>01</sub>    f<sub>c01</sub> = 8.236 GHz  
 P'<sub>21</sub> = 3.054    TE<sub>21</sub>    f<sub>c21</sub> = 10.486 GHz  
 TE<sub>01</sub>    f<sub>c01</sub> = 1.316 GHz

(c) What range of frequencies do you recommend using this waveguide for?

Range of TE<sub>11</sub> mode is 6.32 GHz - TE<sub>21</sub> 10.486 GHz  
 Need to stay in this range. Manufactures chooses above TE<sub>11</sub> and below TE<sub>21</sub> ... 7.27 - 9.97 GHz

(d) Why? TM<sub>01</sub> mode is suppressed by not exciting it (feed system)

(e) How far can you propagate the 9GHz signal on this waveguide before it is attenuated to 50% of its original magnitude?

$$R_s \text{ copper} = \sqrt{\frac{\omega \mu_0}{2\sigma}} = 0.025 \Omega$$

$$\sigma_{cu} = 5.813 \times 10^7 \text{ S/m}$$

$$\alpha = \alpha_c + \alpha_d$$

↑ dielectric loss = 0 in air

$$\alpha_c = \frac{R_s}{ak\eta\beta} \left( k_c^2 + \frac{k^2}{P_{01}^2 - 1} \right) = 0.00447 \text{ Np/m}$$

$$k = \frac{2\pi}{\lambda} \quad k_c =$$

$$e^{-\alpha z} = 0.5$$

$$\beta = \sqrt{k^2 - k_c^2}$$

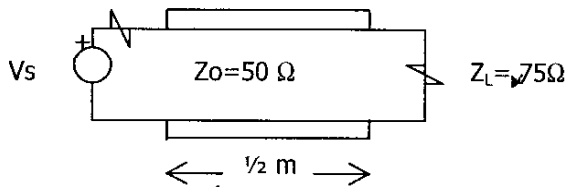
$$z = 139.5 \text{ m}$$

TABLE 4.3. Some standard circular waveguides.

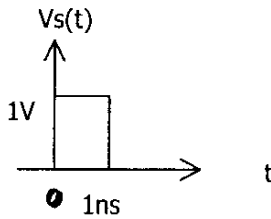
EIA Designation	Inside Dimensions (Inches)			Recommended Frequency Range GHz
	Diameter	Tolerance + or -	Roundness Tolerance	
WC 992	9.915	.010	.010	0.803-1.10
WC 847	8.470	.008	.008	0.939-1.29
WC 724	7.235	.007	.007	1.10-1.51
WC 618	6.181	.006	.006	1.29-1.76
WC 528	5.280	.005	.005	1.51-2.07
WC 451	4.511	.005	.005	1.76-2.42
WC 385	3.853	.004	.005	2.07-2.83
WC 329	3.292	.003	.003	2.42-3.31
WC 281	2.812	.003	.003	2.83-3.88
WC 240	2.403	.0025	.002	3.31-4.54
WC 205	2.047	.002	.002	3.89-5.33
WC 175	1.750	.0015	.0015	4.54-6.23
WC 150	1.500	.0015	.0015	5.30-7.27
WC 128	1.281	.0013	.0013	6.21-8.51
WC 109	1.094	.001	.0011	7.27-9.97
WC 94	0.938	.0009	.0009	8.49-11.6
WC 80	0.797	.0008	.0008	9.97-13.7
WC 69	0.688	.0007	.0007	11.6-15.9
WC 59	0.594	.0006	.0006	13.4-18.4
WC 50	0.500	.0005	.0005	15.9-21.8
WC 44	0.438	.00045	.0004	18.2-24.9
WC 38	0.375	.00038	.0004	21.2-29.1
WC 33	0.328	.00033	.0003	24.3-33.2
WC 28	0.281	.00028	.0001	28.3-38.8
WC 25	0.250	.00025	.0001	31.8-43.6
WC 22	0.219	.00025	.0001	36.4-49.8
WC 19	0.188	.00025	.00007	42.4-58.1
WC 17	0.172	.00025	.00007	46.3-63.5
WC 14	0.141	.00025	.00005	56.6-77.5
WC 13	0.125	.00025	.00005	63.5-87.2
WC 11	0.109	.00025	.00005	72.7-99.7
WC 9	0.094	.00025	.00005	84.8-116

4. A  $50\Omega$  lossy microstripline has  $\alpha = 0.1 \text{ Np/m}$ ,  $V_p = 2 \times 10^8 \text{ m/s}$ ,  $\beta = 0.7 \text{ rad/m}$  and is  $1/2 \text{ m}$  long.

(a) Sketch the time domain voltage at the load for the first 30 ns.  
 $R_g = 100\Omega$



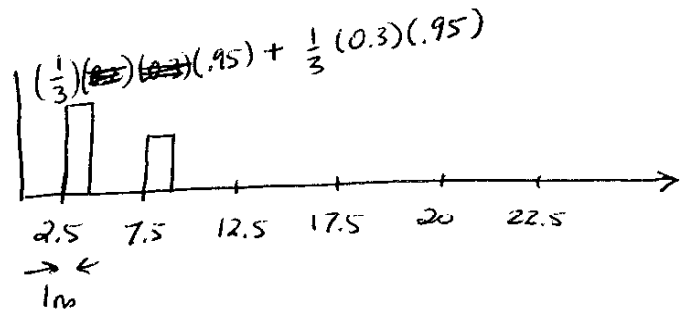
$$T = \frac{d}{v} = \frac{0.5}{2 \times 10^8} = 2.5 \text{ ns}$$



$$V_{in} = V_s \frac{Z_0}{Z_0 + R_g} = \frac{1}{3} \text{ V}$$

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{75 - 50}{75 + 50} = 0.2$$

$$\Gamma_S = \frac{Z_g - Z_0}{Z_g + Z_0} = \frac{100 - 50}{100 + 50} = 0.3$$



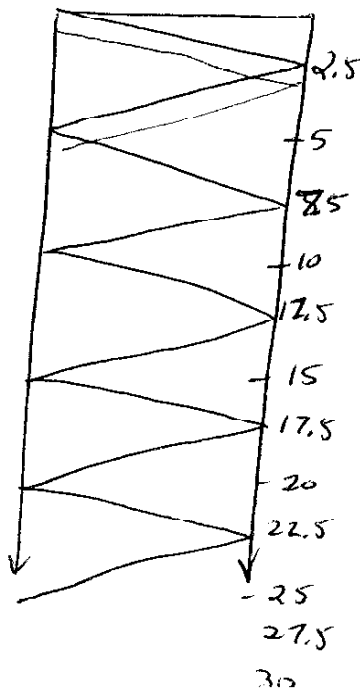
(b) How long (in seconds) do you expect it to be before the pulses observed at the load are less than  $0.01 \text{ V}$  in magnitude?

attenuation

$$e^{-\alpha z} = e^{-(0.1)(0.5)} = 0.95 \text{ each path}$$

~~0.95~~  $e^{-\alpha z} = 0.01 \rightarrow z = 46 \text{ m}$

(c) Sketch the voltage on the line as a function of distance at  $30 \text{ ns}$ .  $t = \frac{z}{v} = 230 \text{ ns}$  | attenuation only



pulses:

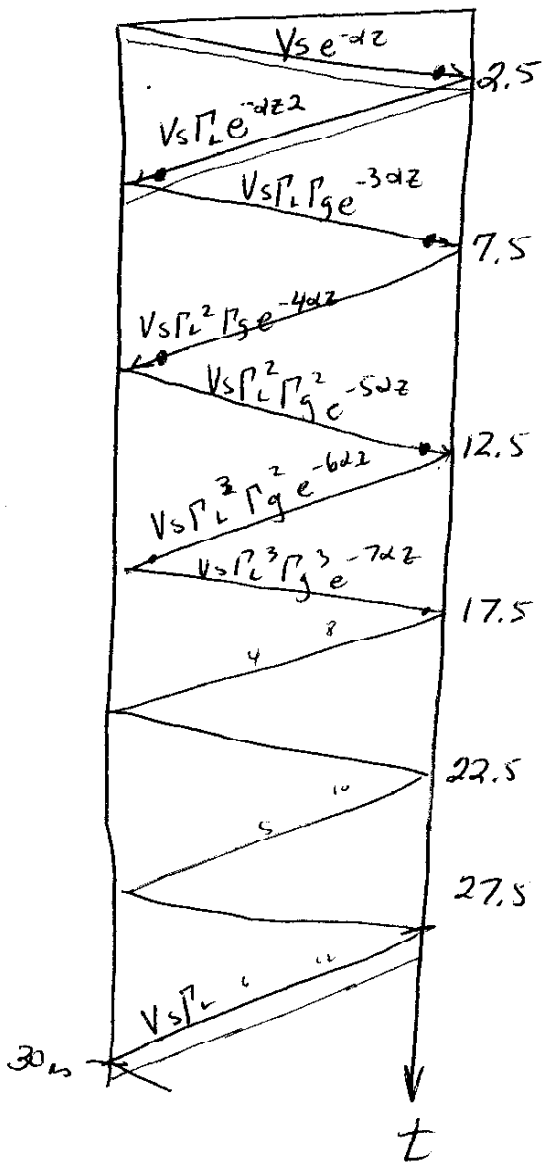
2<sup>nd</sup> pulse will already be below  $0.01 \text{ V}$

$$4) V_{in} = V_s \frac{Z_0}{Z_0 + R_g} = \frac{1}{3} V$$

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{75 - 50}{75 + 50} = 0.9$$

$$\Gamma_g = \frac{Z_g - Z_0}{Z_g + Z_0} = \frac{100 - 50}{100 + 50} = 0.3$$

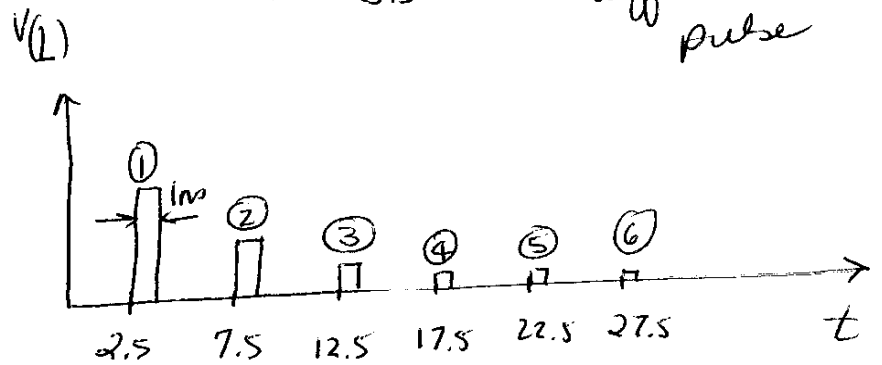
attenuation per trip  $e^{-\alpha z} = e^{-(0.1)(0.5)} = 0.95$



Examine first pulse at load  
 $V_s e^{-\alpha z} + V_s \Gamma_L e^{-\alpha z} = V_s (e^{-\alpha z} + \Gamma_L e^{-\alpha z})$



Neglecting attenuation difference over pulse



$$① V_1 = V_s e^{-\alpha z} + V_s e^{-\alpha z} \Gamma_L = V_s e^{-\alpha z} (1 + \Gamma_L)$$

$$② V_2 = V_s \Gamma_L \Gamma_g e^{-3\alpha z} (1 + \Gamma_L)$$

$$③ V_3 = V_s \Gamma_L^2 \Gamma_g^2 e^{-5\alpha z} (1 + \Gamma_L)$$

$$④ V_4 = V_s \Gamma_L^3 \Gamma_g^3 e^{-7\alpha z} (1 + \Gamma_L)$$

$$⑤ V_5 = V_s \Gamma_L^4 \Gamma_g^4 e^{-9\alpha z} (1 + \Gamma_L)$$

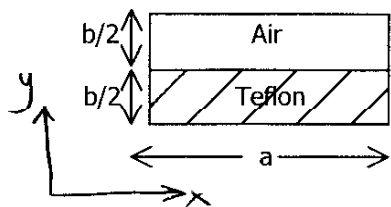
$$⑥ V_6 = V_s \Gamma_L^5 \Gamma_g^5 e^{-11\alpha z} (1 + \Gamma_L)$$

$$z = 0.5m$$

$$V_0 = V_s \Gamma_L^6 \Gamma_g^5 e^{-12\alpha z} + V_s \Gamma_L^6 \Gamma_g^6 e^{-12\alpha z}$$

5. Derive the electric and magnetic fields in the partially-filled WR98 waveguide shown below:

$TE_{0n}$  modes only



For TE modes  $E_z = 0$

For  $0n$  modes  $\partial/\partial x = 0$

$$\left( \frac{\partial^2}{\partial y^2} + k_1^2 \right) H_{z1} = 0 \quad \text{for teflon} \quad 0 \leq y \leq b/2$$

$$\left( \frac{\partial^2}{\partial y^2} + k_2^2 \right) H_{z2} = 0 \quad \text{for air} \quad \frac{b}{2} \leq y \leq b$$

Guess  $H_{z1} = (A_1 \cos k_1 y + B_1 \sin k_1 y) (C_1 \cos k_1 x + D_1 \sin k_1 x)$  on  
 $H_{z2} = (A_2 \cos k_2 y + B_2 \sin k_2 y) (C_2 \cos k_2 x + D_2 \sin k_2 x)$  on

Need  $E_x$  for boundary conditions (remember  $\partial/\partial x = 0$ )

$$\begin{cases} E_{x1} = \frac{-j\omega\mu_0}{k_1^2} \frac{\partial H_{z1}}{\partial y} = \frac{-j\omega\mu_0}{k_1^2} (-A_1 k_1 \sin k_1 y + B_1 k_1 \cos k_1 y) (C_1 \cos k_1 x + D_1 \sin k_1 x) \\ E_{x2} = \frac{-j\omega\mu_0}{k_2^2} (-A_2 k_2 \sin k_2 y + B_2 k_2 \cos k_2 y) (C_2 \cos k_2 x + D_2 \sin k_2 x) \end{cases}$$

Boundary conditions on  $E_x$

$$E_{x1}(y=0) = 0 \rightarrow B_1 = 0 \quad 0 = \frac{j\omega\mu_0}{k_1} (A_1 \sin 0 + B_1 \cos 0)$$

$$E_{x2}(y=b) = 0 \quad 0 = \frac{j\omega\mu_0}{k_2} (A_2 \sin k_2 b - B_2 \cos k_2 b)$$

$$E_{x1}(y=b/2) = E_{x2}(y=b/2) \rightarrow B_2 = 0$$

$$\frac{j\omega\mu_0}{k_1} A_1 \sin k_1 b/2 = \frac{j\omega\mu_0}{k_2} (A_2 \sin k_2 b/2 + B_2 \cos k_2 b/2)$$

$$\left. \begin{aligned} \frac{A_1}{k_1} \sin \frac{k_1 b}{2} &= \frac{A_2}{k_2} \sin \frac{k_2 b}{2} \end{aligned} \right\} \text{Knowing } k_1 \text{ and } k_2 \text{ we could find } A_1/A_2$$



~~Need  $E_y$  for boundary conditions~~

$$\cancel{E_y = \frac{j\omega\mu}{k_1^2} \frac{\partial H_z}{\partial y} = \frac{j\omega\mu}{k_1^2} A_1 k_1 \sin k_1 y}$$

Apply center BC on  $H_z$  also

$$H_{z1}(b/2) = H_{z2}(b/2)$$

$$A_1 \cos k_1 b/2 = A_2 \cos k_2 b/2$$

Combine these equations

$$A_1 \cos b/2 k_1 = A_2 \cos k_2 b/2$$

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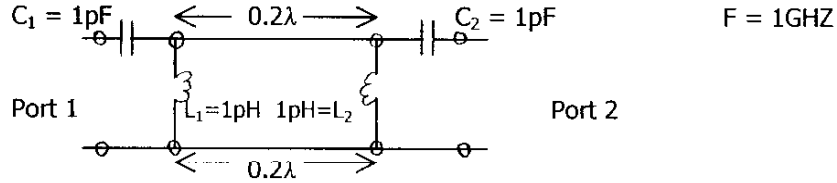
$$\frac{A_1}{k_1} \sin k_1 b/2 = \frac{A_2}{k_2} \sin k_2 b/2$$

$$k_1 \tan k_1 b/2 = k_2 \tan k_2 b/2$$

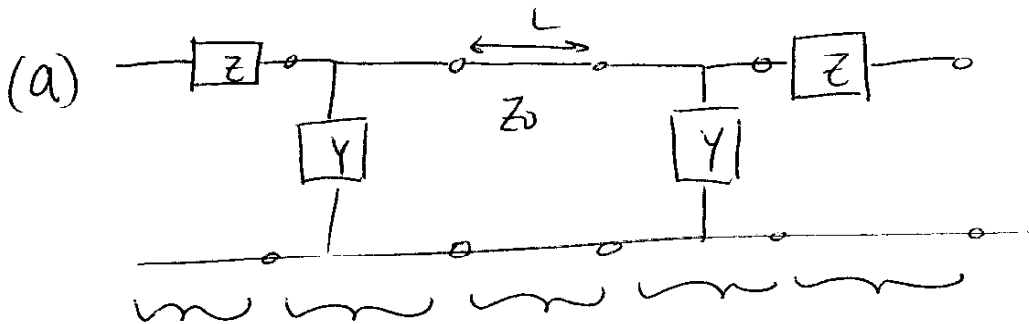
Solve numerically for  $k_1$  &  $k_2$

6.

- (a) Derive the S-parameters for the circuit below. Line lengths not shown are assumed to be zero length.



- (b) If a  $75\Omega$  load is connected to port 2 and a  $1V$  source is input to port 1 ( $V^+ = 1V$ ) how much power is delivered to the load?



ABCD matrices

$$\begin{bmatrix} 1 & 1/j\omega C \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 1/j\omega L \\ 1/j\omega L & 1 \end{bmatrix} \begin{bmatrix} 0.3 & j47.5 \\ j0.019 & 0.3 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 1/j\omega L & 1 \end{bmatrix} \begin{bmatrix} 1 & 1/j\omega C \\ 0 & 1 \end{bmatrix}$$

Using  
Matlab

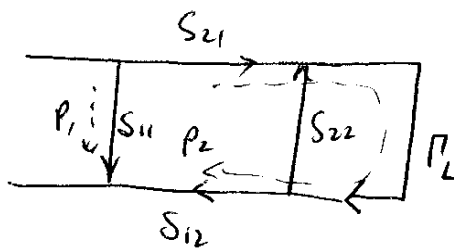
$$= \begin{bmatrix} -0.19 & j3.05 \\ -j.0001 & -0.0192 \end{bmatrix} \times 10^{10}$$

← ABCD

Convert to S =

$$\begin{bmatrix} .8 - j.57 & \sim 0 \\ \sim 0 & .8 - j.57 \end{bmatrix}$$

(b)

Using  
Mason Loop Rules

$$S_{11}' = \frac{S_{11} (1 - S_{22} \Gamma_L) + S_{21} \Gamma_L S_{12} (1 - 0)}{1 - S_{22} \Gamma_L} \approx .82 - j.57$$

$$S_{12}' = \frac{S_{12} (1 - 0)}{1 - S_{22} \Gamma_L} \approx 0$$

$$S_{21}' = \frac{S_{21} (1 - 0)}{1 - S_{22} \Gamma_L} \approx 0$$

$$S_{22}' = \frac{S_{22} (1 - 0)}{1 - S_{22} \Gamma_L} \approx .86 - j.80$$

$$V_2^+ = 0 \quad V_2 = V_2^- = S_{21}' V_1^+ \approx 0$$

$$P = \frac{V_2^2}{Z_L} \approx 0$$

## Grading/Points Possible

**Name** \_\_\_\_\_

Problem 1 \_\_\_\_\_ / 30 points

Problem 2 \_\_\_\_\_ / 35 points

Problem 3 \_\_\_\_\_ / 35 points

Problem 4 \_\_\_\_\_ / 30 points

Problem 5 \_\_\_\_\_ / 40 points

Problem 6 \_\_\_\_\_ / 30 points

**Total** \_\_\_\_\_ / **200 points**