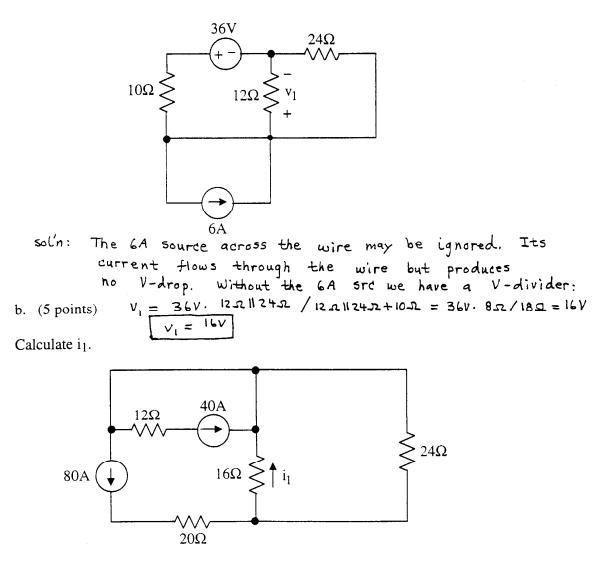


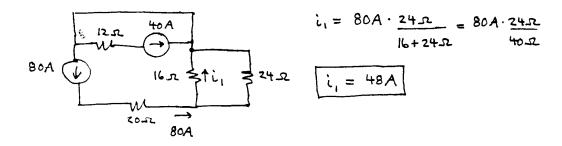
## Review Page 56 of notes - Solution

1. a. (5 points)

Calculate  $v_1$ .

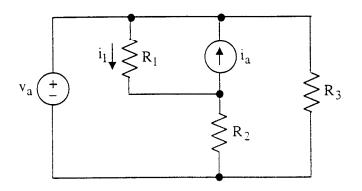






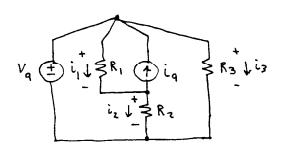
## 2. (30 points)

Derive an expression for  $i_1$ . The expression must not contain more than the circuit parameters  $v_a$ ,  $i_a$ ,  $R_1$ ,  $R_2$ , and  $R_3$ .



sol'n:

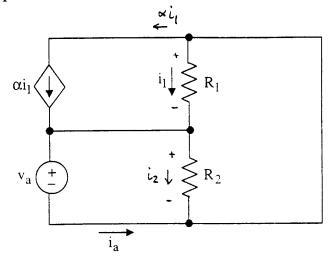
Redraw with top as one node:



Current sum at top or bottom node? No, because we would have to define a current for source  $V_q$ . Current at center node:  $i_q - i_1 + i_2 = 0A$ V-loop around left inner loop:  $V_q - i_1R_1 - i_2R_2 = 0V$ No V-loop for other inner loops because we would have to define V-drop for  $i_q$ . Next larger loop is  $R_1, R_2, R_3: i_2R_2 + i_1R_1 - i_3R_3 = 0V$ New we have 3 perior is 2 is here and no wort to

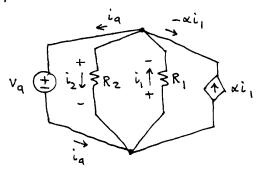
Now we have 3 egns in 3 unknowns, and we want to find  $i_1$ . We observe, however, that the first two egns have only two unknowns. So we don't actually need the 3rd egn. Use  $1^{st}$  eg'n to find  $i_2 = i_1 - i_q$ . Substitute into  $2^{nd}$  eg'n:  $v_q - i_1 R_1 - (i_1 - i_q) R_2 = 0V$ or  $i_1(-R_1 - R_2) = -v_q - i_q R_2$  or  $i_1 = \frac{v_q + i_q R_2}{R_1 + R_2}$ 

- 3. (30 points)
  - a. Derive an expression for  $i_a$ . The expression must not contain more than the circuit parameters  $\alpha$ ,  $v_a$ ,  $R_1$ , and  $R_2$ .



b. Make at least one consistency check (other than a units check) on your expression. Explain the consistency check clearly.

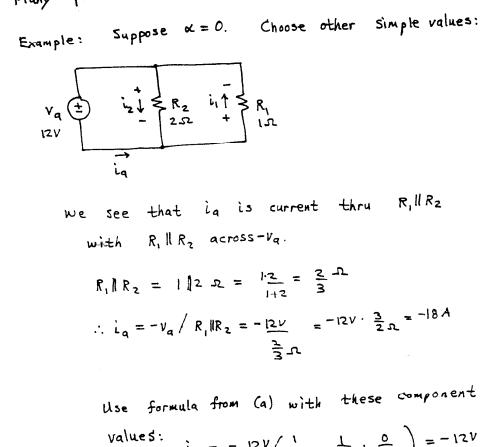
soln: a) Redraw circuit



No current sums at nodes because of Va.

No current for  $V_{a}$  is  $V_{a}$  is  $R_{z} = 0V$  V = 100p on left:  $V_{a} - izR_{z} = 0V$  V = 100p in middle:  $izR_{z} + i_{1}R_{1} = 0V$   $i_{1} = -V_{a}$   $R_{1}$   $V_{a}$  $R_{2}$ 

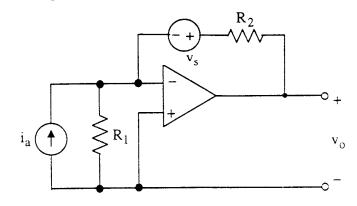
we could also just observe that  $V_a$  is across  $R_i$  and  $R_2$ . Now that we have found  $i_1$  and  $i_2$ , we use a current at top node to find  $i_a$ :  $i_a + i_2 - i_1 - \alpha i_1 = OA$  or  $i_a + \frac{V_a}{R_1} + \frac{v_a}{R_1} = \frac{V_a}{R_1}$ or  $i_a = -\frac{V_a}{R_2} \left(\frac{1}{R_2} + \frac{1}{R_1} + \frac{\alpha}{R_1}\right)$  or  $i_a = -\frac{V_a}{R_1 \|R_1\| \|R_2}$ 



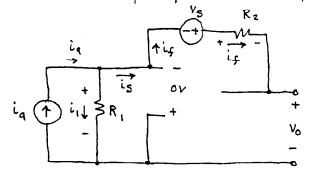
values: 
$$i_{q} = -\frac{12\nu}{2\Omega} \left( \frac{1}{2\Omega} + \frac{1}{1\Omega} + \frac{0}{1\Omega} \right) = -\frac{12\nu \cdot 3}{2}$$

ia = -181 V agrees with obvious solin for this simple case 4. (30 points)

The op-amp operates in the linear mode. Using an appropriate model of the op amp, derive an expression for  $v_0$  in terms of not more than  $v_s$ ,  $i_a$ ,  $R_1$ , and  $R_2$ .



sol'n: Redraw without op-amp and OV drop across + and - inputs: <u>Ys</u> Ro



V-loop on left thru  $R_1$  and OV drop:  $\dot{L}_1 R_1 + OV = OV$  or  $\dot{L}_1 = O$ 

Current sum at node above R1:

V-loop on right thru ov drop, Vs,  $R_2$ , and  $V_0$ :  $-0V + Vs - is R_2 - V_0 = 0V$  or  $is = \frac{Vs - V_0}{R_2}$ Now use is = is. Thus,  $v_0 = 0$ 

$$i_{a} = \frac{v_{s} - v_{o}}{R_{z}} \quad \text{or} \quad v_{o} = v_{s} - i_{a}R_{z}$$