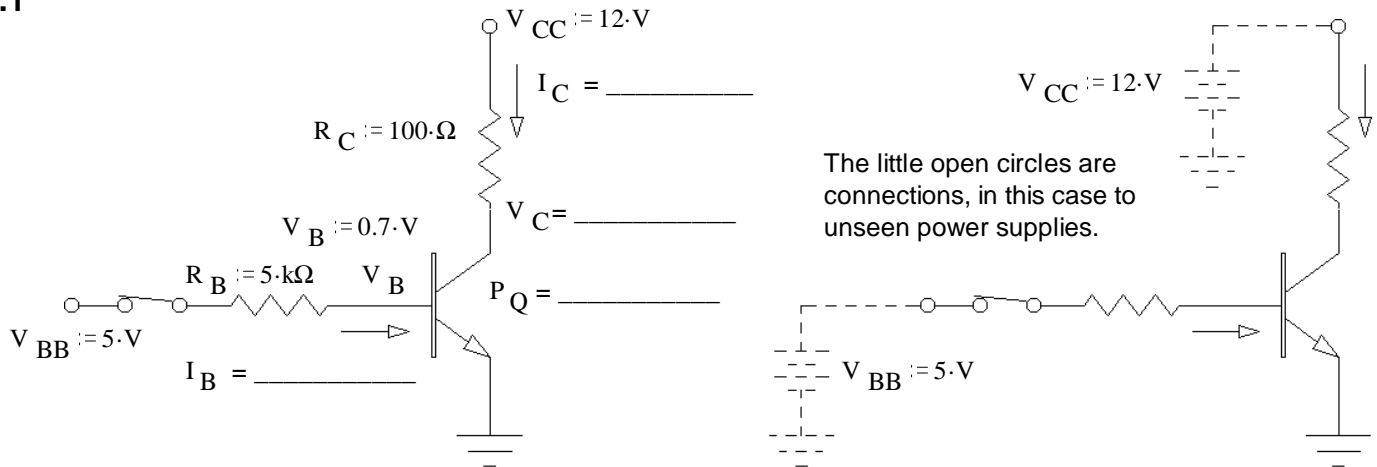


Ex.1



if: $\beta := 100$	$I_B := \frac{V_{BB} - 0.7\text{V}}{R_B}$	$I_B = 0.86 \cdot \text{mA}$	$I_C := \beta \cdot I_B$	$I_C = 86 \cdot \text{mA}$
			$V_C := V_{CC} - R_C \cdot I_C$	$V_C = 3.4 \cdot \text{V}$
			$P_Q := V_C \cdot I_C$	$P_Q = 292.4 \cdot \text{mW}$
if: $\beta := 200$	$I_B := \frac{V_{BB} - 0.7\text{V}}{R_B}$	$I_B = 0.86 \cdot \text{mA}$	$I_C := \beta \cdot I_B$	$I_C = 172 \cdot \text{mA}$
			$V_C := V_{CC} - R_C \cdot I_C$	$V_C = -5.2 \cdot \text{V}$
			must be in saturation:	$V_C := 0.2 \cdot \text{V}$
			$I_C := \frac{V_{CC} - V_C}{R_C}$	$I_C = 118 \cdot \text{mA}$
			$P_Q := V_C \cdot I_C$	$P_Q = 23.6 \cdot \text{mW}$

Since saturation can depend on β , You usually assume a small β when designing a circuit that should saturate (a switching circuit).

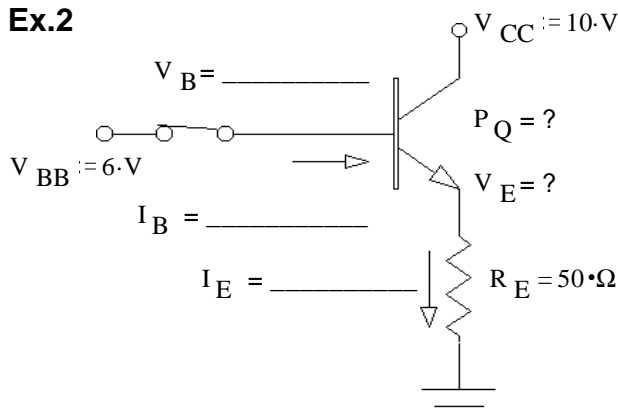
if: $R_C := 50 \cdot \Omega$	$I_C := \beta \cdot I_B$	$I_C = 172 \cdot \text{mA}$	$V_C := V_{CC} - R_C \cdot I_C$	$V_C = 3.4 \cdot \text{V}$
same $\beta := 200$			$P_Q := V_C \cdot I_C$	$P_Q = 584.8 \cdot \text{mW}$

Saturation also depends on R_C and V_{CC} .

What is the largest value that R_B could be and still keep the transistor in saturation?

$$I_{Csat} := \frac{V_{CC} - 0.2\text{V}}{R_C} \quad I_{Csat} = 236 \cdot \text{mA} \quad I_B := \frac{I_{Csat}}{\beta} \quad I_B = 1.18 \cdot \text{mA} \quad R_{Bmax} = \frac{5\text{V} - 0.7\text{V}}{I_B} = 3.644 \cdot \text{k}\Omega$$

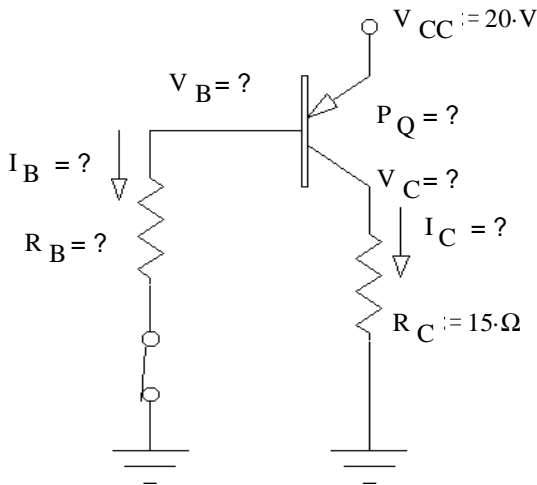
Ex.2



$V_B := 6\text{V}$	$V_E := 5.3\text{V}$	$R_E := 50 \cdot \Omega$
$I_E := \frac{V_E}{R_E}$	$I_E = 106 \cdot \text{mA}$	Doesn't depend on β
$I_B := \frac{I_E}{\beta + 1}$	$I_B = 0.5 \cdot \text{mA} \approx \frac{I_E}{\beta} = 0.53 \cdot \text{mA}$	If β is big enough.
$P_Q := (V_{CC} - V_E) \cdot I_E$	$P_Q = 0.498 \cdot \text{W}$	

ECE 2210 Transistor Switching Circuit Examples, p2

Ex.3 If the load must be connected to ground, a PNP transistor is often a better choice.



Let's assume a small β and saturation and find the R_B necessary.

a small β : $\beta := 20$

$$V_C := V_{CC} - 0.2 \cdot V \quad V_C = 19.8 \cdot V$$

$$R_C := 15 \cdot \Omega$$

$$I_{C_{sat}} := \frac{V_C}{R_C} \quad I_{C_{sat}} = 1.32 \cdot A$$

$$I_B := \frac{I_{C_{sat}}}{\beta} \quad I_B = 66 \cdot mA$$

$$V_B := V_{CC} - 0.7 \cdot V \quad V_B = 19.3 \cdot V$$

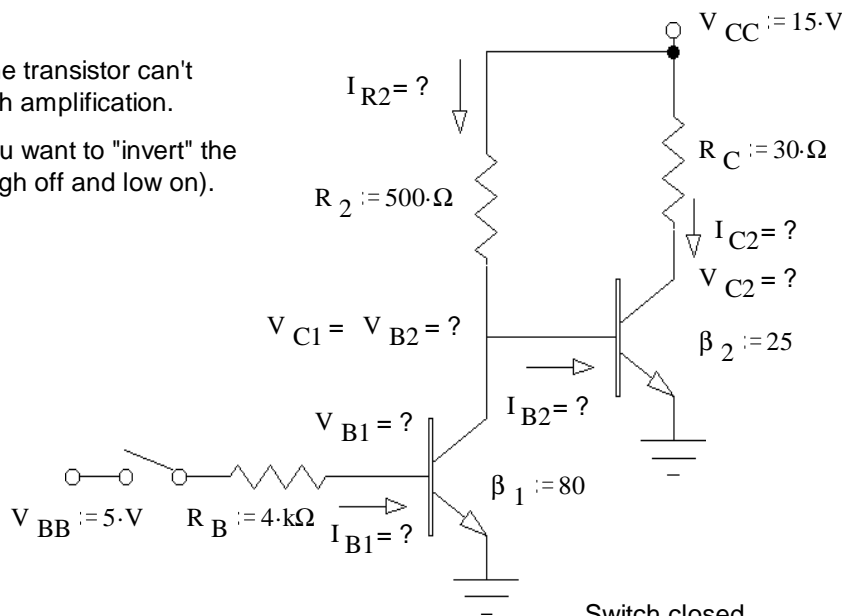
$$R_B := \frac{V_B}{I_B} \quad R_B = 292 \cdot \Omega$$

$$P_Q := 0.2 \cdot V \cdot I_{C_{sat}} \quad P_Q = 264 \cdot mW$$

Ex.4

Sometimes one transistor can't provide enough amplification.

Sometimes you want to "invert" the input (make high off and low on).



Switch open

$$I_{B1o} := 0 \quad V_{B1o} := 0 \cdot V$$

$$V_{B2o} := 0.7 \cdot V$$

$$I_{B2o} := \frac{V_{CC} - 0.7 \cdot V}{R_2} \quad I_{B2o} = 28.6 \cdot mA$$

$$I_{R2o} := I_{B2o} \quad I_{R2o} = 28.6 \cdot mA$$

$$I_{C2o} := \beta_2 \cdot I_{B2o} \quad I_{C2o} = 715 \cdot mA$$

$$V_{C2o} := V_{CC} - R_C \cdot I_{C2o} \quad V_{C2o} = -6.45 \cdot V$$

$$Q_2 \text{ must be in saturation: } \quad V_{C2o} := 0.2 \cdot V$$

$$I_{C2o} := \frac{V_{CC} - V_{C2o}}{R_C} \quad I_{C2o} = 493.3 \cdot mA$$

Switch closed

$$I_{B1c} := \frac{5 \cdot V - 0.7 \cdot V}{R_B} \quad I_{B1c} = 1.08 \cdot mA$$

$$\text{assume } Q_1 \text{ is in saturation} \quad V_{C1c} := 0.2 \cdot V$$

$$I_{C1c} := \frac{V_{CC} - V_{C1c}}{R_2} \quad I_{C1c} = 29.6 \cdot mA$$

$$\beta_1 \cdot I_{B1c} = 86 \cdot mA \quad I_{C1} \text{ is controlled by } R_2$$

$$V_{B2c} := V_{C1c} \quad V_{B2c} = 0.2 \cdot V$$

$$I_{B2c} := 0 \quad I_{C2c} := 0 = I_{RCc}$$

When the switch is open, current flows in through the load resistor, R_C . When it is closed, no current flows through the load. This is an example of logical "inversion".

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Ex.5 Modified from F07 Final

A transistor is used to control the current flow through an inductive load (in the dotted box, it could be a relay coil or a DC motor).

a) Assume the transistor is in saturation (fully on) and that switch has been closed for a long time. What is the load current?

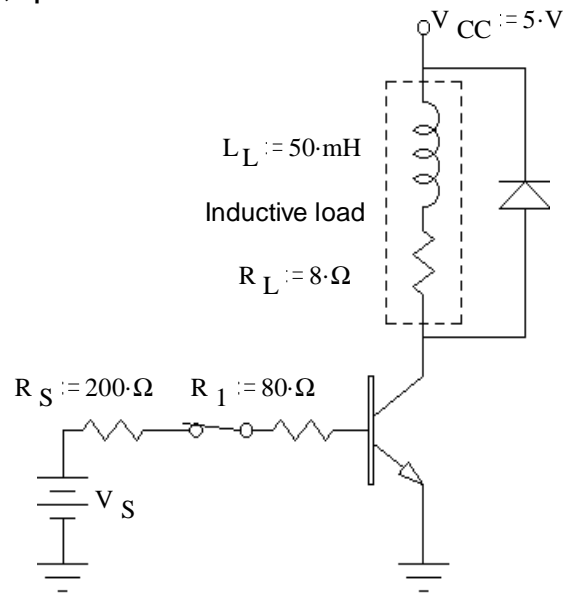
$$I_C = ?$$

$$I_{Csat} := \frac{V_{CC} - 0.2 \cdot V}{R_L} \quad I_{Csat} = 600 \cdot \text{mA}$$

b) $\beta := 80$ find the minimum value of V_S , so that the transistor will be in saturation.

$$I_{Bmin} := \frac{I_{Csat}}{\beta} \quad I_{Bmin} = 7.5 \cdot \text{mA}$$

$$V_{Smin} := I_{Bmin} \cdot (R_S + R_1) + 0.7 \cdot V \quad V_{Smin} = 2.8 \cdot V$$



Use this V_S for the rest of the problem.

c) Does the diode in this circuit ever conduct a significant current? If yes, when and how much?

$$\text{When the switch opens.} \quad I_{Dmax} = I_{Csat} = 600 \cdot \text{mA} \quad \text{from part a)}$$

d) You got a bad transistor. $\beta := 60$ Find the new I_C , and V_{CE} and P_Q .

$$I_C = ? \quad I_C := \beta \cdot I_{Bmin} \quad I_C = 450 \cdot \text{mA} \quad \text{Now operating in active region}$$

$$V_{CE} = ? \quad V_{CE} := V_{CC} - R_L \cdot I_C \quad V_{CE} = 1.4 \cdot V$$

$$P_Q = ? \quad P_Q := V_{CE} \cdot I_C \quad P_Q = 0.63 \cdot W$$

$\beta = 60$ Use this for the rest of the problem.

c) Find the minimum value of R_L so that the transistor will be in saturation.

$$I_B := \frac{V_{Smin} - 0.7 \cdot V}{R_S + R_1} \quad I_B = 7.5 \cdot \text{mA}$$

$$I_{Cmax} := \beta \cdot I_B \quad I_{Cmax} = 450 \cdot \text{mA}$$

$$R_{Lmin} := \frac{V_{CC} - 0.2 \cdot V}{I_{Cmax}} \quad R_{Lmin} = 10.7 \cdot \Omega$$

d) R_L , can't be changed, so find the maximum value of R_1 so that the transistor will be in saturation.

$$I_{Csat} = 600 \cdot \text{mA} \quad \text{from part a)}$$

$$I_{Bmin} := \frac{I_{Csat}}{\beta} \quad I_{Bmin} = 10 \cdot \text{mA}$$

$$R_{1max} = \frac{V_{Smin} - 0.7 \cdot V}{I_{Bmin}} - R_S = 10 \cdot \Omega$$

ECE 2210 Transistor Switching Circuit Examples, p4

Ex.6 From F05 Final with modifications from F06 Final

A transistor is used to control the current flow through an inductive load (in the dotted box, it could be a relay coil or a DC motor).

- a) $\beta := 25$ Assume the transistor is in the active region, find I_{sw} , I_L , V_L , V_{EC} and P_Q .

$$I_B := \frac{V_S - 0.7 \cdot V}{R_S + R_1} \quad I_B = 18.6 \cdot \text{mA} = I_{sw}$$

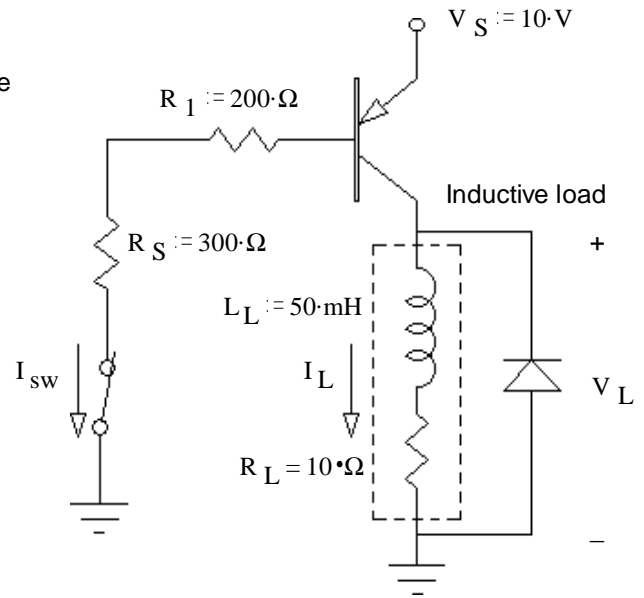
$$I_L := \beta \cdot I_B \quad I_L = 465 \cdot \text{mA}$$

$$R_L := 10 \cdot \Omega$$

$$V_L := I_L \cdot R_L \quad V_L = 4.65 \cdot V$$

$$V_{EC} := V_S - V_L \quad V_{EC} = 5.35 \cdot V$$

$$P_Q := V_{EC} \cdot I_L \quad P_Q = 2.488 \cdot W$$



- b) Was the transistor actually operating in the active region? yes no (circle one) yes

How do you know? (Specifically show a value which is or is not within a correct range.)

$$V_{EC} = 5.35 \cdot V > 0.2 \cdot V$$

- c) Find the maximum value of R_1 , so that the transistor will be in saturation.

If saturated: $V_{EC} := 0.2 \cdot V$

$$I_{Csat} := \frac{V_S - 0.2 \cdot V}{R_L} \quad I_{Csat} = 0.98 \cdot A$$

$$I_{Bmin} := \frac{I_{Csat}}{\beta} \quad I_{Bmin} = 39.2 \cdot \text{mA}$$

$$R_{1max} = \frac{V_S - 0.7 \cdot V}{I_{Bmin}} - R_S = -63 \cdot \Omega \quad \text{NOT POSSIBLE}$$

- d) $R_1 = 200 \cdot \Omega$ and can't be changed, find the minimum value of β so that the transistor will be in saturation.

$$I_{Csat} = 0.98 \cdot A \quad \beta_{min} := \frac{I_{Csat}}{I_B} \quad \beta_{min} = 52.7$$

- e) How much power is dissipated by the transistor if it has the β you found in part d)

$$P_Q := 0.2 \cdot V \cdot I_{Csat} \quad P_Q = 0.196 \cdot W$$

- f) Does the diode in this circuit ever conduct a significant current? If yes, when and how much?

When the switch opens. $I_{Dmax} = I_{Csat} = 0.98 \cdot A$ from part a)

- g) The switch is open for a while. What is the load current (I_L) now? 0

ECE 2210 Transistor Switching Circuit Examples, p5

Ex.7 From F13 Final

Transistors are used to control the current flow through an inductive load (in the dotted box, it could be a relay coil or a DC motor).

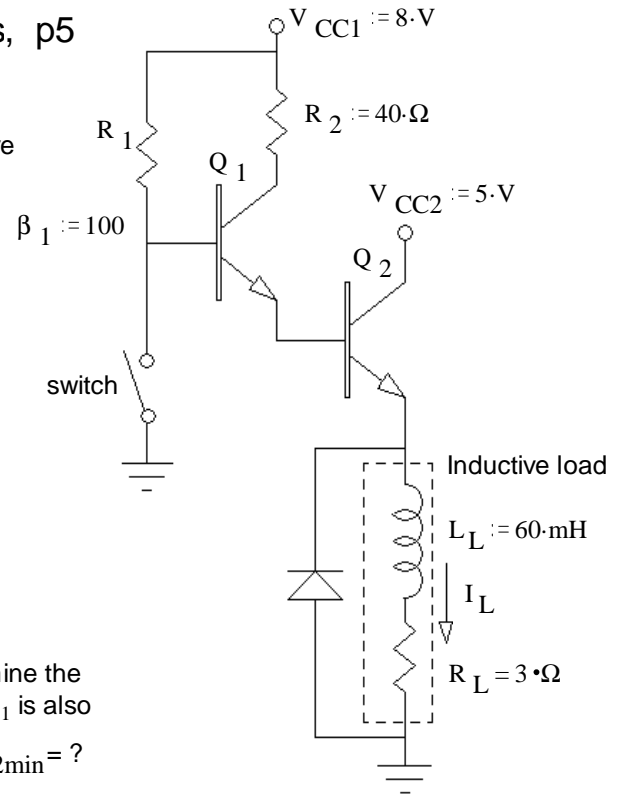
- a) In order for current to flow in through the load, the switch should be: i) closed or ii) open (Circle one)
- b) Assume the switch has been in the position you circled above for a long time. I_L is 1.3A. Find the power dissipated by transistor Q_2 (neglect base current and V_{BE}).

$$I_L := 1.3 \cdot A \quad P_{Q2} = ? \quad R_L := 3 \cdot \Omega$$

$$V_{CE2} := V_{CC2} - I_L \cdot R_L \quad V_{CE2} = 1.1 \cdot V$$

$$P_{Q2} := V_{CE2} \cdot I_L \quad P_{Q2} = 1.43 \cdot W$$

- c) This is an unacceptable power loss, so you would like to determine the minimum β_2 needed so that Q_2 will be in saturation. Assume Q_1 is also in saturation. You may assume $I_E = I_C$ for both transistors.



$$\beta_{2min} = ?$$

$$I_L := \frac{V_{CC2} - 0.2 \cdot V}{R_L} \quad I_L = 1.6 \cdot A = I_{C2}$$

$$V_{E2} := V_{CC2} - 0.2 \cdot V \quad V_{E2} = 4.8 \cdot V$$

$$V_{B2} := V_{E2} + 0.7 \cdot V \quad V_{B2} = 5.5 \cdot V$$

$$V_{C1} := V_{B2} + 0.2 \cdot V \quad V_{C1} = 5.7 \cdot V$$

$$I_{C1} := \frac{V_{CC1} - V_{C1}}{R_2} \quad I_{B2} := I_{C1} \quad I_{B2} = 57.5 \cdot mA \quad \beta_{2min} = \frac{I_L}{I_{B2}} = 27.826$$

Better answer

$$I_{B2} := I_{C1} \cdot \left(\frac{\beta_1 + 1}{\beta_1} \right) \quad I_{B2} = 58.075 \cdot mA \quad \beta_{2min} = \frac{I_L}{I_{B2}} - 1 = 26.551$$

You replace Q_2 with a new transistor that has a β greater than what you just calculated.

- d) How much power is dissipated by the new transistor Q_2 (neglect base current and V_{BE})? $P_{Q2} = ?$

$$P_{Q2} := 0.2 \cdot V \cdot I_L \quad P_{Q2} = 320 \cdot mW$$

- e) What is the maximum value of R_1 needed to saturate Q_1 ? $\beta_1 = 100$

$$I_{B1min} := \frac{I_{C1}}{\beta_1} \quad I_{B1min} = 0.575 \cdot mA \quad V_{B1} := V_{B2} + 0.7 \cdot V \quad V_{B1} = 6.2 \cdot V$$

$$R_{1max} := \frac{V_{CC1} - V_{B1}}{I_{B1min}} \quad R_{1max} = 3.13 \cdot k\Omega$$

- f) Does the diode in this circuit ever conduct a significant current? If yes, when and how much?

When the switch closes. $I_{Dmax} = I_L = 1.6 \cdot A$ from part c)

ECE 2210 Transistor Switching Circuit Examples, p6

Ex.8 From F12 Final

A couple of transistors are used to control the current flow through an inductive load. The switch has been closed, as shown, for a long time.

- a) You measure the voltage at each collector (referenced to ground) as shown on the drawing. Find the power dissipated by transistor Q_2 .

$$V_{C1} := 5 \cdot V \quad V_{C2} := 2 \cdot V$$

$$I_L := \frac{V_{CC} - 2 \cdot V}{R_L} \quad I_L = 1.5 \cdot A$$

$$P_{Q2} := V_{C2} \cdot I_L \quad P_{Q2} = 3 \cdot W$$

- b) Find the β of transistor Q_2 .

$$V_{R2} := 5 \cdot V - 0.7 \cdot V \quad V_{R2} = 4.3 \cdot V$$

$$I_{R2} := \frac{V_{R2}}{R_2} \quad I_{R2} = 43 \cdot mA$$

$$\beta_2 := \frac{I_L}{I_{R2}} \quad \beta_2 = 34.884$$

- c) Find the β of transistor Q_1 .

$$I_{R1} := \frac{V_{CC} - 0.7 \cdot V}{R_1} \quad \beta_1 := \frac{I_{R2}}{I_{R1}} \quad \beta_1 = 58.9$$

- d) Find the minimum β for transistor Q_1 to be in saturation. $\beta_{1min} = ?$

$$\text{If } Q_1 \text{ is saturated: } V_{R2} := V_{CC} - 0.2 \cdot V - 0.7 \cdot V \quad V_{R2} = 7.1 \cdot V$$

$$\text{If } Q_1 \text{ is saturated: } I_{R2} := \frac{V_{R2}}{R_2} \quad I_{R2} = 71 \cdot mA \quad \beta_{1min} := \frac{I_{R2}}{I_{R1}} \quad \beta_{1min} = 97.3$$

You replace Q_1 with a different transistor so that now: $\beta_1 := 200$ Use this from now on.

- e) Find the new load current (I_L) assuming transistor Q_2 is in the active region.

$$Q_1 \text{ is saturated: } I_{R2} = 71 \cdot mA \quad I_L := I_{R2} \cdot \beta_2 \quad I_L = 2.477 \cdot A$$

- f) Check the assumption that Q_2 is in the active region and recalculate I_L if necessary.

$$I_{R2} \cdot \beta_2 \cdot R_L = 9.907 \cdot V \quad V_{CE2} := V_{CC} - I_{R2} \cdot \beta_2 \cdot R_L \quad V_{CE2} = -1.907 \cdot V \quad \text{Not possible}$$

$$Q_2 \text{ is saturated: } I_L := \frac{V_{CC} - 0.2 \cdot V}{R_L} \quad I_L = 1.95 \cdot A$$

- g) Does the diode in this circuit ever conduct a significant current? If yes, when and how much?

$$\text{When the switch opens. } I_{Dmax} = 1.95 \cdot A \quad \text{from part f)}$$

