## Notes. Second Order Transients

ECE 2210 A.Stolp 4/6/00, 3/16/07 final conditions Laplace DC AC Capacitor impedance initial conditions 1 open  $\frac{1}{\mathbf{C} \cdot \mathbf{s}}$ short, or  $j \cdot \omega \cdot C$  $v_{C}(0+) = v_{C}(0-)$ Inductor  $v_{L} = L \frac{d}{dt} i_{L}$   $i_{L} = \frac{1}{L} \begin{vmatrix} c \\ c \\ v_{L} dt \end{vmatrix}$ <u>\_</u>\_\_\_\_\_ L·s open, or short j·ω·L  $i_{I}(0+) = i_{I}(0-)$ Resistor  $v_R = i_R \cdot R$   $i_R = \frac{v_R}{R}$  $\neg \land \land \land$ R R R R Characteristic equation Use Laplace impedances, manipulate your circuit equation(s) into one equation of this form: May be  $I_{in}$  or any forcing function / May be  $I_X$  or any desired variable  $(a_1 \cdot s^2 + b_1 \cdot s + k_1) \cdot \mathbf{V}_{in}(s) = (s^2 + b \cdot s + k) \cdot \mathbf{V}_{\mathbf{X}}'(s)$  with NO denominator s terms a1, b1, k1 coefficients may be zero  $s^2 + b \cdot s + k = 0$  is the characteristic equation **Differential equation**  $a_1 \cdot \frac{d^2}{dt^2} v_{in}(t) + b_1 \cdot \frac{d}{dt} v_{in}(t) + k_1 \cdot V_{in}(t) = \frac{d^2}{dt^2} v_X(t) + b \cdot \frac{d}{dt} v_X(t) + k \cdot v_X(t)$ **ransfer function** Rearrange circuit equation to:  $\mathbf{H}(s) = \frac{\text{output}}{\text{input}} = \frac{\mathbf{V} \mathbf{X}(s)}{\mathbf{V} \mathbf{in}(s)} = \frac{a_1 \cdot s^2 + b_1 \cdot s + k_1}{s^2 + b \cdot s + k} = \text{transfer function}$   $s^2 + b \cdot s + k = 0$ Characteristic equation of the second sec Transfer function characteristic equation Complete solution Solutions to the characteristic equation:  $s_1 = -\frac{b}{2} + \frac{\sqrt{b^2 - 4 \cdot k}}{2}$   $s_2 = -\frac{b}{2} - \frac{\sqrt{b^2 - 4 \cdot k}}{2}$ **Find initial Conditions** (v<sub>C</sub> and/or  $i_L$ ) Find conditions of just before time t = 0,  $v_C(0)$  and  $i_L(0)$ . These will be the same just after time t = 0,  $v_C(0)$  and  $i_L(0)$ and will be your initial conditions. Use normal circuit analysis to find your desired variable:  $v_{\mathbf{X}}(0)$  or  $i_{\mathbf{X}}(0)$ Also find:  $\frac{d}{dt}v_X(0)$  or  $\frac{d}{dt}i_X(0)$  The trick to finding these is to see that:  $\frac{d}{dt}v_C(0) = \frac{{}^1C^{(0)}}{C}$  and  $\frac{d}{dt}i_L(0) = \frac{{}^vL^{(0)}}{T}$ Find final conditions ("steady-state" or "forced" solution) DC inputs: Inductors are shorts Capacitors are opens Solve by DC analysis  $v_X(\infty)$  or  $i_X(\infty)$ AC inputs: Solve by AC steady-state analysis using jo X(t) may be replaced by  $v_{\rm X}(t),\,i_{\rm X}(t)$  or any desired variable in the equations below Overdamped  $b^2 - 4 \cdot k > 0$  $s_1$  and  $s_2$  are real and negative typical  $X(t) = X(\infty) + B \cdot e^{s \cdot 1 \cdot t} + D \cdot e^{s \cdot 2 \cdot t}$ time  $X(0) = X(\infty) + B + D$   $\frac{d}{dt}X(0) = B \cdot s_1 + D \cdot s_2$  Solve simultaneously for B and D <u>Critically damped</u>  $b^2 - 4 \cdot k = 0$   $s_1 = s_2 = -\frac{b}{2} = s$   $s_1$  and  $s_2$  are typical real, equal and time  $X(t) = X(\infty) + B \cdot e^{s \cdot t} + D \cdot t \cdot e^{s \cdot t}$ negative  $\frac{d}{dt}X(0) = B \cdot s + D \qquad \text{so.. } D = \frac{d}{dt}X(0) - B \cdot s$  $X(0) = X(\infty) + B$ so., B =  $X(0) - X(\infty)$  $s_1 = \alpha + j \cdot \omega$   $s_2 = \alpha - j \cdot \omega$   $\alpha$  is negative  $s_1 + D \cdot sin(\omega \cdot t)$  complex  $s_1$  and  $s_2$ typical Underdamped  $b^2 - 4 \cdot k < 0$  $e^{\alpha \cdot t}$ α is negative  $X(t) = X(\infty) + e^{\alpha \cdot t} (B \cdot \cos(\omega \cdot t) + D \cdot \sin(\omega \cdot t))$  $\frac{d}{dt}X(0) = B \cdot \alpha + D \cdot \omega \quad \text{so.. } D = \frac{\frac{d}{dt}X(0) - B \cdot \alpha}{C}$ time  $X(0) = X(\infty) + B$ so.. B =  $X(0) - X(\infty)$ ω

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