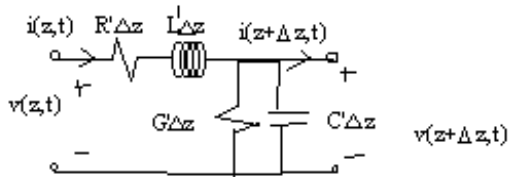


## ECE3300 -- LECTURE 6

### Transmission Line Equations (Telegraphers Equations):



Lumped element model represents voltage and current on transmission line. Voltage and current?? What about fields??? Fortunately, they are dual (proportional).

#### **Kirchoff Loop Equation:**

$$V(z,t) - R I(z,t) - L \frac{di(z,t)}{dt} - v(z+\Delta z,t) = 0$$

$$R = R' \Delta z, \quad L = L' \Delta z$$

Divide by  $\Delta z$ , combine V terms, and rearrange:

$$V(z,t) / \Delta z - R' I(z,t) - L' \frac{dI(z,t)}{dt} - V(z+\Delta z,t) / \Delta z = 0$$

$$-[ V(z+\Delta z,t) - V(z,t) ] / \Delta z = R' I(z,t) + L' \frac{dI(z,t)}{dt}$$

Limit as  $\Delta z \rightarrow 0$  (difference goes to differential):

$$-\frac{dV(z,t)}{dz} = R' I(z,t) + L' \frac{dI(z,t)}{dt}$$

#### **Kirchoff Node Equation:**

$$I(z,t) - G v(z+\Delta z,t) - C \frac{dv(z+\Delta z,t)}{dt} - I(z+\Delta z,t) = 0$$

$$I(z,t) - G' \Delta z v(z+\Delta z,t) - C' \Delta z \frac{dv(z+\Delta z,t)}{dt} - I(z+\Delta z,t) = 0$$

Divide by  $\Delta z$  and rearrange :

$$-[ I(z+\Delta z,t) - I(z,t) ] / \Delta z = G' v(z+\Delta z,t) + C' \frac{dv(z+\Delta z,t)}{dt}$$

Limit as  $\Delta z \rightarrow 0$  :

$$-\frac{dI(z,t)}{dz} = G' v(z+\Delta z,t) + C' \frac{dv(z+\Delta z,t)}{dt}$$

#### **Telegraphers equations:**

$$-\frac{dV(z,t)}{dz} = R' I(z,t) - L' \frac{dI(z,t)}{dt}$$

$$-\frac{dI(z,t)}{dz} = G' v(z+\Delta z,t) + C' \frac{dv(z+\Delta z,t)}{dt}$$

### Sinusoidal Steady-State Form:

Convert to Phasor form.

$$-dV(z)/dz = (R' + j\omega L') I(z)$$

$$-dI(z)/dz = (G' + j\omega C') V(z)$$

What is difference between this and “regular” circuit equations?? They are a function of  $z$ ... distance down the transmission line.

### Wave Equation form:

Take  $d/dz$  of one equation, and substitute it into the other equation. (Doesn't matter which one)

$$-d^2 I(z)/dz^2 = (G' + j\omega C') dV(z)/dz$$

$$dV(z)/dz = -d^2 I(z)/dz^2 / (G' + j\omega C')$$

$$-dV(z)/dz = (R' + j\omega L') I(z)$$

$$-d^2 I(z)/dz^2 / (G' + j\omega C') = (R' + j\omega L') I(z)$$

$$-d^2 I(z)/dz^2 - ((R' + j\omega L') (G' + j\omega C')) I(z) = 0$$

$$-d^2 I(z)/dz^2 - \gamma^2 I(z) = 0$$

alternate form (derived in text)

$$-d^2 V(z)/dz^2 - \gamma^2 V(z) = 0$$

### Complex Propagation Constant:

$$\gamma = \sqrt{(R' + j\omega L') (G' + j\omega C')} = \alpha + j \beta$$

### attenuation constant:

$$\alpha = \text{Re}[(R' + j\omega L') (G' + j\omega C')] \text{ (Neper/meter)}$$

Passive Lines (all shown here) = zero or positive ...  $\exp(-\alpha z)$  attenuation occurs

Active Lines (active region of laser) = negative ... gain occurs

### Phase constant

$$\beta = \text{Im}[(R' + j\omega L') (G' + j\omega C')] \text{ (radians/meter)}$$

phase shift term

### Forward and Backward Waves

Solutions of the basic wave equations have solutions of the form:

$$V(z) = V_o^+ e^{-\gamma z} + V_o^- e^{\gamma z} \text{ volts}$$

$$I(z) = I_o^+ e^{-\gamma z} + I_o^- e^{\gamma z} \text{ amps}$$

Later, we will see:

$e^{-\gamma z}$  represents forward(+) traveling wave

$e^{\gamma z}$  represents backward(-) traveling wave

### Characteristic Impedance

$$d/dz [V(z)] = d/dz [V_o^+ e^{-\gamma z} + V_o^- e^{\gamma z} \text{ volts}] = \gamma [V_o^+ e^{-\gamma z} + V_o^- e^{\gamma z} \text{ volts}]$$

Plug into wave equation:

$$\gamma [-V_o^+ e^{-\gamma z} + V_o^- e^{\gamma z} \text{ volts}] = (R' + j\omega L')I(z)$$

$$I(z) = \gamma [V_o^+ e^{-\gamma z} - V_o^- e^{\gamma z} \text{ volts}] / (R' + j\omega L') = [\gamma / (R' + j\omega L')] [V_o^+ e^{-\gamma z} - V_o^- e^{\gamma z} \text{ volts}]$$

$$Z_o = V_o^+ / I_o^+ = V_o^- / I_o^- = (R' + j\omega L') / \gamma = \text{sqrt}((R' + j\omega L') / (G' + j\omega C'))$$

Characteristic impedance is the ratio of V/I for forward and backward waves, SEPARATELY. It is not the ration of V/I for the total wave.

$$V_o^+ = |V_o^+| e^{j\phi^+}$$

$$V_o^- = |V_o^-| e^{j\phi^-}$$

$$\begin{aligned} v(z,t) &= \text{Real}(V(z) e^{j\omega t}) = \text{Real}[(V_o^+ e^{-\gamma z} + V_o^- e^{\gamma z}) e^{j\omega t}] \\ &= \text{Real}[|V_o^+| e^{j\phi^+} e^{j\omega t} e^{-(\alpha + j\beta)z} + |V_o^-| e^{j\phi^-} e^{j\omega t} e^{(\alpha + j\beta)z}] \\ &= |V_o^+| e^{-\alpha z} \cos(\omega t - \beta z + \phi^+) + |V_o^-| e^{\alpha z} \cos(\omega t + \beta z + \phi^-) \end{aligned}$$

First term: Traveling wave in +z direction (coefficients of t and z have opposite signs)

Second term: Traveling wave in -z direction (coefficients have same signs)

$$\text{Propagation Velocity: } v_p = \omega / \beta = f \lambda$$

### Standing Wave (next section):

Combination of +z and -z traveling waves

**Example:** (exercise 2.4)

A 2-wire air line has  $R'=.404$  mohm/m,  $L'=2. \mu\text{H/m}$ ,  $G'=0$ ,  $C'=5.56$  pF  
For operation at 5 kHz, determine

(a) Attenuation constant

$$\begin{aligned} \alpha &= \text{Re}[\text{sqrt}((R' + j\omega L')(G' + j\omega C'))] = 3.37 \times 10^{-7} \text{ Np/m} \\ \omega &= 2\pi f = 2\pi \times 5 \times 10^3 \end{aligned}$$

(b) Phase constant

$$\beta = \text{Im}[\text{sqrt}((R' + j\omega L') / (G' + j\omega C'))] = 1.05 \times 10^{-4} \text{ rad/m}$$

(c) Phase velocity

$$v_p = \omega / \beta = 2.99 \times 10^8 \text{ m/s}$$

(d) Characteristic impedance

$$Z_o = \text{sqrt}((R' + j\omega L') / (G' + j\omega C')) = 600 - j2 \text{ ohms} = 600 \angle -0.19^\circ \text{ ohms}$$

How would you increase  $Z_o$  using the same materials?

$R'$  is function of resistance of conductors. Using same materials, you would need MORE metal to increase this. Make wires thicker.

$L'$  is function of inductance between conductors. Bring them closer together to increase  $L'$ .

$C'$  similar, but want to decrease it to increase  $Z_o$ .... TRADEOFFS!