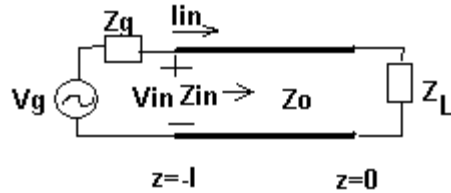


ECE 3300 INPUT IMPEDANCE

Input Impedance

$$Z_{in}(z) = V(z) / I(z)$$



$Z_{in}(z)$ is ratio of TOTAL voltage $V(z)$ and current $I(z)$ on line.

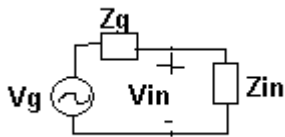
Z_o is ratio of forward or negative traveling wave V_o^+ / I_o^+ or V_o^- / I_o^-

$$\begin{aligned} Z_{in}(z) &= V(z) / I(z) \\ &= V_o^+ [e^{-j\beta z} + \Gamma e^{j\beta z}] / (V_o^+ / Z_o) [e^{-j\beta z} - \Gamma e^{j\beta z}] \\ &\text{Divide by } e^{-j\beta z} \\ &= Z_o [1 + \Gamma e^{j2\beta z}] / [1 - \Gamma e^{j2\beta z}] \text{ ohm} \end{aligned}$$

$$\begin{aligned} Z_{in}(\text{at the generator}) &= Z_{in}(z = -l) \\ &= Z_o [1 + \Gamma e^{-j2\beta l}] / [1 - \Gamma e^{-j2\beta l}] \text{ ohm} \end{aligned}$$

Using: $e^{j\beta l} = \cos(\beta l) + j \sin(\beta l)$ and $e^{-j\beta l} = \cos(\beta l) - j \sin(\beta l)$

$$\begin{aligned} Z_{in}(-l) &= Z_o [Z_L \cos(\beta l) + j Z_o \sin(\beta l)] / [Z_o \cos(\beta l) + j Z_L \sin(\beta l)] \\ &= Z_o [Z_L + j Z_o \tan(\beta l)] / [Z_o + j Z_L \tan(\beta l)] \end{aligned}$$



Voltage Divider for Input Voltage

$$V_{in} = I_{in} Z_{in} = V_g Z_{in} / (Z_g + Z_{in})$$

$$V_{in} = V(-l) = V_o^+ [e^{j\beta l} + \Gamma e^{-j\beta l}]$$

$$\text{Solve for } V_o^+ = [V_g Z_{in} / (Z_g + Z_{in})] / [e^{j\beta l} + \Gamma e^{-j\beta l}]$$

Now we know the positive traveling wave based on the generator voltage!

Remember we found relation for V_o^- from V_o^+ last time.

Given the generator voltage and impedance and the load impedance, we can now completely solve for the voltages (and currents) everywhere on the transmission line.

Example: Complete Solution

There is one example in your text. Here is a different one.

Given: a lossless transmission line

$$Z_0 = 50 \text{ ohms}$$

Length = 90 meters

$$V_p = 3e8 \text{ m/s (air-filled transmission line)}$$

Source: 2 GHz generator with $R_g = 150 \text{ ohms}$ connected to input terminal

Load: Output terminal left open $R_L = \infty$

$$\lambda = v_p / f = 3e8 / 2e9 = 0.15 \text{ m}$$

$$\beta = 2\pi / \lambda = 41.89 \text{ rad/m}$$

Voltage Reflection Coefficient (at the load)

$$\Gamma = (\infty - 50) / (\infty + 50) = 1 \angle 0$$

Input Impedance

$$Z_{in} = Z_0 [Z_L + j Z_0 \tan(\beta l)] / [Z_0 + j Z_L \tan(\beta l)] = 0 - j 45 \text{ ohms}$$

Generator voltage

$$v_g(t) = 10 \sin(\omega t + 30^\circ) \text{ volts}$$

convert to cosine

$$v_g(t) = 10 \cos(\omega t + (30-90)^\circ) \text{ volts}$$

convert to phasor

$$V_g = 10 \angle -60^\circ \text{ volts}$$

Input voltage (total voltage at input terminal)

$$V_{in} = V_g Z_{in} / (Z_{in} + R_g) = (4) (-j 45) / (-j 45 + 150) = 2.87 \angle 46.7^\circ \text{ Volt}$$

Magnitude of Forward-traveling wave

$$V_o^+ = V_{in} / [e^{j\beta l} + \Gamma e^{-j\beta l}] = 2.14 \angle 46.7^\circ \text{ Volt}$$

$|V_o^+|$ may be $\leftrightarrow |V_{in}|$

Phasor (total) Voltage

$$V(z) = V_o^+ [e^{-j\beta z} + \Gamma e^{j\beta z}] = 3.20 \angle 180^\circ [e^{-j\beta z} + 1 \angle 0 e^{j\beta z}]$$

Instantaneous (total) Voltage

$$v(z,t) = \text{Real} [V(z)] = 3.20 \cos(\omega t - \beta z + 180^\circ) + 3.20 \cos(\omega t + \beta z + 180^\circ) \text{ volts}$$

Phasor (total) Current

$$I(z) = (V_o^+ / Z_0) [e^{-j\beta z} - \Gamma e^{j\beta z}]$$

$$= (3.20 \angle 180^\circ / 50) [e^{-j\beta z} - 1 \angle 0 e^{j\beta z}] = 0.64 \angle 180^\circ [e^{-j\beta z} - e^{j\beta z}]$$

Instantaneous (total) Current

$$i(z,t) = 0.64 \cos(\omega t - \beta z + 180^\circ) + 0.64 \cos(\omega t + \beta z + 180^\circ) \text{ amps}$$

Electrical Length

Why did $Z_{in} = Z_0$? Because line is electrically so long that generator doesn't "see" the load.

Electrical Length = length / wavelength = 900 meters / .15 meters = 6000 wavelengths long.

What if this generator had been a battery? (DC)

Then wavelength = ∞

$$\beta = 0$$

$$\tan(\beta l) = 0$$

$$Z_{in} = Z_0 [Z_L + j Z_0 \tan(\beta l)] / [Z_0 + j Z_L \tan(\beta l)]$$

$$= 50 [\infty + 0] / [50 + 0] = \infty = Z_L!$$

The line is electrically so SHORT that it is invisible, and the input impedance of the line is the load. This is exactly what happens when you are considering "ordinary" (low frequency) circuits.

Transient Effects

Does this mean there will be NO reflection?? No. There will be a reflection, when the wave finally reaches the end.

BUT? Our cos functions show the incident and reflected waves simultaneously. There is no 6000 cycle delay shown here!

That's because the phasor solution is a STEADY STATE solution. Transients and transient effects are not shown. Are transient effects important? Yes. We'll learn about them next week.

Summary of Lossless Transmission Lines

Lossless Transmission Line

$$R' \ll \omega L', G' \ll \omega C'$$

$$\gamma = \alpha + j \beta = j \omega \sqrt{L' C'}$$

$$\alpha = 0$$

$$\beta = \omega \sqrt{L' C'}$$

$$Z_0 = \sqrt{L' / C'} \rightarrow \text{strictly real}$$

$$\lambda = 2\pi / \beta = 2\pi / \omega \sqrt{L' C'}$$

$$v_p = \omega / \beta = 1 / \sqrt{L' C'}$$

For TEM line:

$$L' C' = \mu \epsilon \text{ (properties of insulation material)}$$

Lossless TEM line:

$$\beta = \omega / \sqrt{\mu\epsilon}$$

$$v_p = 1 / \sqrt{\mu\epsilon} = c_0 / \sqrt{\epsilon_r}$$

$$\lambda = v_p / f = \lambda_0 / \sqrt{\epsilon_r}$$

Phasor (total steady-state) voltage and current

$$V(z) = V_0^+ e^{-j\beta z} + V_0^- e^{j\beta z}$$

$$= V_0^+ e^{-j\beta z} + \Gamma V_0^+ e^{j\beta z}$$

$$I(z) = (V_0^+ / Z_0) e^{-j\beta z} - (V_0^- / Z_0) e^{j\beta z}$$

$$= (V_0^+ / Z_0) [e^{-j\beta z} - \Gamma e^{j\beta z}]$$

Voltage and Current at Load

$$Z_L = V_L / I_L = [(V_0^+ + V_0^-) / (V_0^+ - V_0^-)] * Z_0$$

$$V_L = V(z=0) = V_0^+ + V_0^-$$

$$I_L = I(z=0) = V_0^+ / Z_0 - V_0^- / Z_0$$

Voltage Reflection Coefficient (at load)

$$\Gamma = V_0^- / V_0^+$$

$$= [(Z_L - Z_0) / (Z_L + Z_0)]$$

$$= (Z_L / Z_0 - 1) / (Z_L / Z_0 + 1)$$

$$= |\Gamma| \angle \theta_r = |\Gamma| e^{j\theta_r}$$

$$= (S-1) / (S+1)$$

Current Reflection Coefficient (at load)

$$I_0^- / I_0^+ = - V_0^- / V_0^+ = - \Gamma$$

Magnitude of voltage maxima:

$$|V(z)|_{\max} = |V_0^+| [1 + |\Gamma|]$$

Location of voltage maxima:

$$-z = l_{\max} = (\theta_r \lambda / 4\pi + n\lambda / 2) \text{ for } n=1,2,\dots \text{ if } \theta_r < 0; n=0,1,2,\dots \text{ if } \theta_r \geq 0$$

$$\text{First voltage Maximum: } L_{\max} = \theta_r \lambda / 4\pi$$

Location of voltage minima:

$$L_{\min} = (-(2n+1)\pi + \theta_r) / 2\beta$$

First minima at n=0.

Voltage Standing Wave Ratio (VSWR):

$$S = |V|_{\max} / |V|_{\min} = (1 + |\Gamma|) / (1 - |\Gamma|) \text{ dimensionless}$$

Input Impedance

$$Z_{\text{in}}(z) = V(z) / I(z)$$

$$= Z_0 [1 + \Gamma e^{j2\beta z}] / [1 - \Gamma e^{j2\beta z}] \text{ ohm}$$

$$Z_{\text{in}}(\text{at the generator}) = Z_{\text{in}}(z = -l)$$

$$= Z_0 [1 + \Gamma e^{-j2\beta l}] / [1 - \Gamma e^{-j2\beta l}] \text{ ohm}$$

$$= Z_0 [Z_L + j Z_0 \tan(\beta l)] / [Z_0 + j Z_L \tan(\beta l)]$$

Input Voltage

$$V_{in} = I_{in} Z_{in} = V_g Z_{in} / (Z_g + Z_{in})$$

$$V_{in} = V(-l) = V_o^+ [e^{j\beta l} + \Gamma e^{-j\beta l}]$$

Positive-traveling wave

$$V_o^+ = [V_g Z_{in} / (Z_g + Z_{in})] / [e^{j\beta l} + \Gamma e^{-j\beta l}]$$

Negative-traveling wave

$$V_o^- = [(Z_L - Z_0) / (Z_L + Z_0)] * V_o^+$$