## ECE 3510 Final Exam Study Guide

The Final will be open book, open notes exam with calculators.

## The exam will cover

1. Laplace transforms (simple forms only)
2. Inverse Laplace transforms (partial fractions)
3. Relationship of signals to pole locations

Figs $2.1 \& 2.2$ on page 7
4. Boundedness and convergence of signals

Bounded if all poles in LHP, no double poles on j $\omega$-axis
Converges to 0 if all poles LHP. Converges to a non-zero value if a single pole is at zero
5. $\mathrm{H}(\mathrm{s})$ of circuits
$\mathrm{Z}(\mathrm{s}) \quad \mathrm{R} \quad \mathrm{Ls} \quad \frac{1}{\mathrm{Cs}}$
Be able to find $\frac{\mathrm{V}_{\text {out }(\mathrm{s})}^{\mathrm{V}_{\mathrm{in}}(\mathrm{s})}}{\text { 列 }}$ or any other output over input. Review voltage dividers and current dividers
6. Block Diagrams \& their transfer functions. Standard feedback loop transfer function
7. BIBO Stability (Systems)

BIBO if all poles in LHP, no poles on $j \omega$-axis
8. Impulse \& step responses
$\mathrm{h}(\mathrm{t}) \quad \frac{1}{\mathrm{~s}} \cdot \mathrm{H}(\mathrm{s})$

9. Steady-state (DC gain) \& transient step responses $\mathrm{H}(0)$
10. Effects of pole locations on step response, see Fig 3.12, p.36.
11. Steady-state sinusoidal response. You should be ready to do some complex arithmetic. $\mathrm{H}(\mathrm{j} \omega)$
12. Transient sinusoidal response. You should be ready to do partial fraction expansion to the first (transient) term.

$$
\begin{array}{rrr}
H(s) \quad & \mathrm{A} \cdot \frac{\mathrm{~s}}{\mathrm{~s}^{2}+\omega^{2}} & \text { or }
\end{array} \mathrm{B} \mathrm{\cdot} \mathrm{\frac{} \mathrm { \omega }{s^{2}+\omega^{2}}} \begin{aligned}
\mathrm{A} \cdot \cos (\omega \mathrm{t}) & \mathrm{B} \cdot \sin (\omega \mathrm{t})
\end{aligned}
$$

13. Effect of initial conditions
$Y(s)=\frac{\mathrm{b}_{2} \cdot \mathrm{~s}^{2}+\mathrm{b}_{1} \cdot \mathrm{~s}+\mathrm{b}_{0}}{\mathrm{~s}^{2}+\mathrm{a}_{1} \cdot \mathrm{~s}+\mathrm{a}_{0}} \cdot \mathrm{X}(\mathrm{s}) \quad+\frac{\mathrm{s} \cdot \mathrm{y}(0)+\frac{\mathrm{d}}{\mathrm{dt}} \mathrm{y}(0)+\mathrm{a}_{1} \cdot \mathrm{y}(0)-\mathrm{b}_{2} \cdot \mathrm{~s} \cdot \mathrm{x}(0)-\mathrm{b}_{2} \cdot \mathrm{~s} \cdot \frac{\mathrm{~d}}{\mathrm{dt}} \mathrm{x}(0)-\mathrm{b}_{1} \cdot \mathrm{~s} \cdot \mathrm{x}(0)}{\mathrm{s}^{2}+\mathrm{a}_{1} \cdot \mathrm{~s}+\mathrm{a}_{0}}$
May ask question like points on p. 42
May give $H(s)$, a's \& b's and $y(0) .$. and ask for effect of initial conditions
14. The advantages of state space over classical frequency-domain techniques.

Multiple input / multiple output systems
Can model nonlinear systems
Can model time varying systems
Can be used to design optimal control systems
Can determine controllability and observability

## EDE 3510 Final Exam Study Guide p2

15. Electrical analogies of mechanical systems, particularly translational and rotational systems.

Review the handout and homeworks 8 \& 9 .
16. Control system characteristics and the objectives of a "good" control system. See pg. 57-58

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Stable
Tracking
    fast
    smooth
    minimum error (often measured in steady state)
```

Reject disturbances
Insensitive to plant variations
Tolerant of noise
17. Elimination of steady-state error, p. 61.

DC

1 System stable
$2 \mathrm{C}(\mathrm{s})$ or $\mathrm{P}(\mathrm{s})$ has pole @ 0
3 No zero @ 0

1 System stable
2 Chs) has pole @ 0
3 or $\mathrm{P}(\mathrm{s})$ has zero @ 0 But bad for above
19. Routh-Hurwitz method.

$$
\mathrm{D}(\mathrm{~s})=\mathrm{s}^{3}+20 \cdot s^{2}+59 \cdot \mathrm{~s}+32
$$

Be able to do this with variable such as " k "

| $\mathrm{s}^{3}$ | 1 | 59 |
| :---: | :---: | :---: |
| $\mathrm{~s}^{2}$ | 20 | 32 |
| $\mathrm{~s}^{1}$ | $\frac{20 \cdot 59-1 \cdot 32}{20}=57.4$ | $\frac{20 \cdot 0-1 \cdot 0}{20}=0$ |
| $\mathrm{~s}^{0}$ | $\frac{57.4 \cdot 32-20 \cdot 0}{57.4}=32$ | $\frac{57.4 \cdot 0-20 \cdot 0}{57.4}=0$ |

20. Root - Locus method
a) Main rules
21. Root-locus plots are symmetric about the real axis.
22. On the real axis, spaces left of an odd number of O-L poles and zeros are always part of the locus. (Essentially, every other space on the real axis (counting leftward) is part of the plot.)
23. Each O-L pole originates $(\mathrm{k}=0)$ one branch.

Each O-L zero terminates ( $\mathrm{k}=\infty$ ) one branch. (m)
All remaining branches go to $\infty$.
( $\mathrm{n}-\mathrm{m}$ )
These remaining branches approach asymptotes as they go to $\infty$.
4. The origin of the asymptotes is the centroid.

5. The angles of the asymptotes

| $\_\mathrm{n}-\mathrm{m}$ | angles (degrees) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 2 | 90 | 270 |  |  |
| 3 | 60 | 180 | 300 |  |
| 4 | 45 | 135 | 225 | 315 |$>$

6. The angles of departure (and arrival) of the locus are almost always:


OR:


ICE 3510 Final Exam Study Guide p2
b) Additional Root locus rules. Review the handout.

1. The breakaway points are also solutions to: $\sum_{\text {all }} \frac{1}{\left(\mathrm{~s}+-\mathrm{p}_{\mathrm{i}}\right)}=\sum_{\text {all }} \frac{1}{\left(\mathrm{~s}+-\mathrm{z}_{\mathrm{i}}\right)}$
2. Gain at any point on the root locus: $\quad k=\frac{1}{|G(s)|}$
3. Phase angle of $G(s)$ at any point on the root locus: $\quad \arg (\mathrm{G}(\mathrm{s}))=\arg (\mathrm{N}(\mathrm{s}))-\arg (\mathrm{D}(\mathrm{s}))= \pm 180^{\circ} \pm 360^{\circ} \ldots$

$$
\text { Or: } \quad \arg \left(\frac{1}{\mathrm{G}(\mathrm{~s})}\right)=\arg (\mathrm{D}(\mathrm{~s}))-\arg (\mathrm{N}(\mathrm{~s}))= \pm 180^{\circ} \quad \pm 360^{\circ} \ldots
$$

4. Departure angles from complex poles: $180-90-153.4+135=71.6 \mathrm{deg}$

Root Locus general

a) Concepts of what a root locus plot is and what it tells you. Movement of poles
b) Good vs bad, fast response vs slow, OK damping vs bad.
c) Effects of adding a compensator
d) Important conclusions from root locus, section 4.4.5, p. 82.
e) Simple root-locus design, the placement of additional poles and zeros in order to affect the root locus.
21. Phase-locked loops

How does it work The loop block diagram Material from labs
22. Bode Plots

Be able to draw both magnitude and phase plots
I may ask you to start with a circuit
Basic rules
Complex poles an zeros

$$
\mathrm{s}^{2}+2 \cdot \zeta \cdot \omega_{\mathrm{n}} \cdot \mathrm{~s}+\omega_{\mathrm{n}}{ }^{2}
$$

$$
(s+a)^{2}+b^{2}=s^{2}+2 \cdot a \cdot s+a^{2}+b^{2}
$$

$\max$ at $\quad \omega_{\mathrm{n}} \quad \frac{1}{2 \cdot \zeta}$
Bode to transfer function (like problem 5.2b)
GM \& PM
23. Nyquist plots

You may be asked to draw one, be able to find start, end, and end approach angle.
Use a quicky Bode plot to estimate curve
Concepts of what a Nyquist plot is and what it tells you. $\quad \mathrm{Z}=\mathrm{N}+\mathrm{P}$ Make sure you understand problem 5.11 GM \& PM
24. Phase-lead compensator

1. Discrete signals $\mathrm{x}(\mathrm{k})$
2. z-transform $X(z)=\sum_{k=0}^{\infty} x(k) \cdot z^{-k}$

Finite-length signals have all poles at zero
3. Relationship of signals to pole locations, Fig 6.9, p155. lines of constant damping Speed of decay
4. Properties of the z-transform

$$
\begin{aligned}
& \text { linear } \\
& \text { Right-shift = delay }=\text { multiply by } \quad \mathrm{z}^{-1}=\frac{1}{\mathrm{z}} \\
& \text { Left-shift = advance }=\text { multiply by } \mathrm{z} \\
& \text { Initial value }=\mathrm{x}(0)=\mathrm{X}(\infty) \\
& \text { Final value }(\mathrm{DC})=\mathrm{x}(\infty)=(\mathrm{z}-1) \cdot \mathrm{X}(\mathrm{z})
\end{aligned}
$$

5. Inverse z-transforms (partial fractions \& long division)

Divide by z first:

$$
\begin{array}{ccc}
\frac{\mathrm{X}(\mathrm{z})}{\mathrm{z}} & \mathrm{~A} & \mathrm{~A} \cdot \delta(\mathrm{k}) \\
\text { Poles on real axis (not at zero) } & \frac{\mathrm{B} \cdot \mathrm{z}}{(\mathrm{z}-\mathrm{p})} & \mathrm{B} \cdot \mathrm{p}^{\mathrm{k}} \\
\text { Complex poles } & \frac{\mathrm{B} \cdot \mathrm{z}}{(\mathrm{z}-\mathrm{p})}+\frac{\overline{\mathrm{B}} \cdot \mathrm{z}}{(\mathrm{z}-\overline{\mathrm{p}})} & 2 \cdot|\mathrm{~B}| \cdot(|\mathrm{p}|)^{\mathrm{k}}
\end{array}
$$

6. Boundedness and convergence of signals, relate to continuous-time signals

Bounded if all poles in inside unit circle, no double poles on unit circle
Converges to 0 if all poles inside unit circle. Converges to a non-zero value if a single pole is at 1
7. Difference equations, be able to get $\mathrm{H}(\mathrm{z})$
8. Discrete-time systems, FIR (all poles at zero), IIR (some poles not at zero)
9. BIBO Stability, all poles inside unit circle.
10. Step \& Sinusoidal responses, effects of poles \& zeros, etc.

$$
\text { DC gain }=\mathrm{H}(1) \quad \text { sinusoidal: } \mathrm{H}\left(\mathrm{e}^{\left.\mathrm{j} \cdot \Omega_{\mathrm{o}}\right)}=|\mathrm{H}| \underline{\theta}_{\mathrm{H}} \quad\right. \text { multiply magnitudes and add angles }
$$

11. Initial Conditions, p. 174
12. Implementations, p176 \& 177, be able to go back and forth to $\mathrm{H}(\mathrm{z})$
13. Same Feedback system as in continuous-time and Root locus works the same but is interpreted very differently.
14. Sampled-data systems $\quad t=k \cdot T \quad x_{d}(k)=x(k T) \quad A / D$ converter $\quad z=e^{s \cdot T} \quad s=\frac{\ln (z)}{T}$

Compare s-plane to z-plane, Fig 7.3, p. 190
15. Conversions of continuous-time transfer functions to discrete-time transfer functions

$$
\begin{aligned}
& y(s)=\frac{1}{s} \cdot H(s) \quad \text { find } y(t) \text { by partial frac. exp. } \quad y_{d}(k)=y(k T) \quad \text { find: } Y(z) \quad \frac{z}{z-1} \cdot H(z)=Y(z) \\
& \text { step response discrete step response } \\
& \text { 16. Nyquist sampling criterion, at least twice the highest signal frequency } \\
& \mathrm{H}(\mathrm{z})=\frac{\mathrm{z}-1}{\mathrm{z}} \cdot \mathrm{Y}(\mathrm{z})
\end{aligned}
$$

All Homeworks I' II scan through for problems

## All Labs

Position \& speed control DC motor characteristics PID

PLL

Matlab
Ball \& Beam Inverted Pendulum

Discrete system should have the same step response

