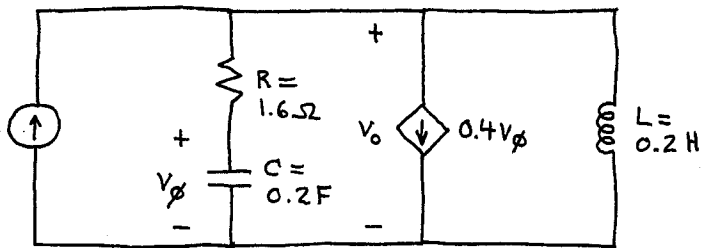


ex:

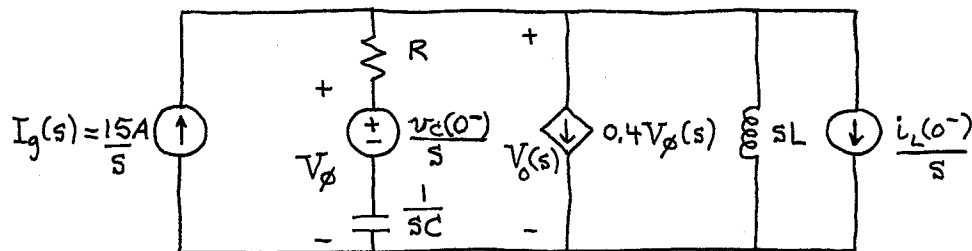
$$i_g(t) = 15u(t) \text{ A}$$



Find $v_o(t)$. $v_c(0^-) = 12\text{V}$, $i_L(0^-) = 5\text{A}$ flowing down

$$\text{ans: } v_o(t) = -51.6te^{-5t} + 20.32e^{-5t} \text{ V}$$

sol'n: We transform the circuit to the s-domain by
 1) taking the Laplace transform of $i_g(t)$,
 2) taking " " " " " L and C, and
 3) including sources for initial condition in L and C.

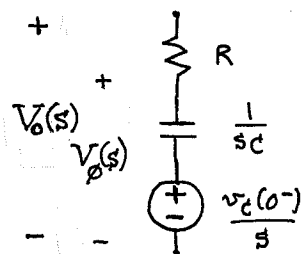


At this point, we may use Node-voltages, current meshes, Thevenin equivalents, or any other method that we would apply when solving a problem involving impedances.

Superposition is particularly useful since we may find the response of the circuit to each source, including those for initial conditions.

Since we have a dependent source, we first define V_ϕ in terms of node voltage(s).

We rearrange the branch containing V_ϕ :



The voltage across R and $\frac{1}{sC}$ is

$$V_0(s) - \frac{v_c(0^-)}{s}$$

We use this

voltage in the voltage divider formula to find the voltage across $\frac{1}{sC}$:

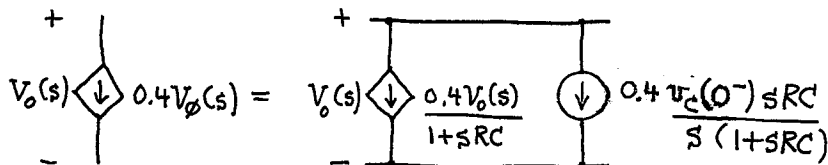
$$V_c(s) = \left[V_0(s) - \frac{v_c(0^-)}{s} \right] \frac{1/sC}{R + 1/sC}$$

Adding $V_c(s)$ to $\frac{v_c(0^-)}{s}$ gives $V_\phi(s)$:

$$V_\phi(s) = V_0(s) \frac{1/sC}{R + 1/sC} + \frac{v_c(0^-)}{s} \left(\frac{-1/sC}{R + 1/sC} + 1 \right)$$

$$\text{or } V_\phi(s) = V_0(s) \frac{1}{1 + sRC} + \frac{v_c(0^-)}{s} \frac{sRC}{1 + sRC}$$

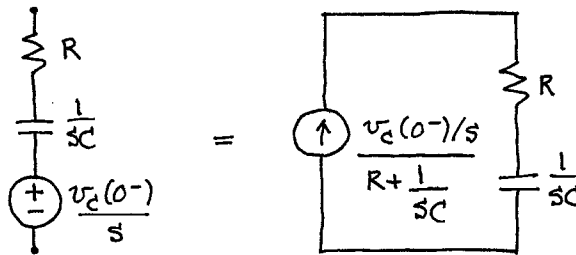
At this point, we observe that we may represent the dependent current source as two current sources that sum to produce current $0.4V_\phi(s)$:



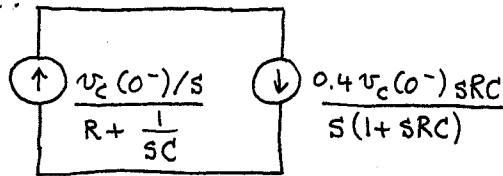
The leftmost of the two sources is equivalent to an impedance, $Z = V/I$:

$$Z = \frac{V_0(s)}{\frac{0.4V_0(s)}{1+sRC}} = \frac{1+sRC}{0.4} \Omega$$

Because we already have four current sources in parallel, it is convenient to convert the branch containing the C from its Thevenin form to a Norton equivalent form.

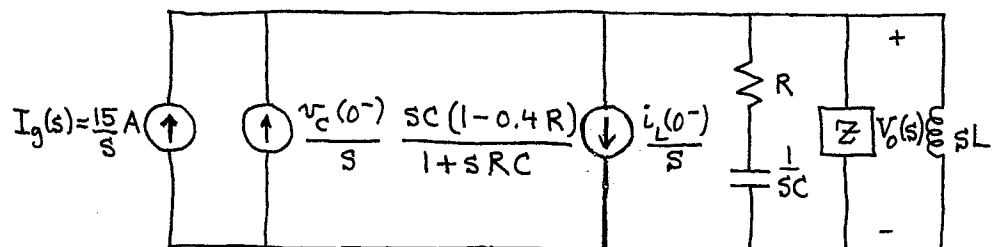


We may combine the current source from this Norton equivalent with the independent source from the equivalent circuit for the dependent source:



$$= \uparrow \frac{v_c(0^-)}{s} \left[\frac{sC - 0.4sC \cdot R}{1 + sRC} \right]$$

Combining all of the above results and putting current sources together, we have a final model:



Now we have $V_o(s) = I_{Tot}(s) \cdot Z_{Tot}(s)$.

We calculate Z_{Tot} using the following identity for impedances written as $z_i(s) = b_i(s)/a_i(s)$ where $b_i(s)$ and $a_i(s)$ are polynomials in s :

$$\begin{aligned} z_1 \parallel z_2 \parallel \dots \parallel z_N &= \frac{b_1(s)}{a_1(s)} \parallel \frac{b_2(s)}{a_2(s)} \parallel \dots \parallel \frac{b_N(s)}{a_N(s)} \\ &= b_1(s) \cdot b_2(s) \cdot \dots \cdot b_N(s) \\ &\quad \cdot \frac{1}{a_1(s)b_2(s)\dots b_N(s)} \parallel \frac{1}{a_2(s)b_1(s)b_3(s)\dots b_N(s)} \\ &\quad \parallel \dots \parallel \frac{1}{a_N(s)b_1(s)\dots b_{N-1}(s)} \\ &= \frac{b_1(s)b_2(s)\dots b_N(s)}{a_1(s)b_2(s)\dots b_N(s) + a_2(s)b_1(s)b_3(s)\dots b_N(s) \\ &\quad + \dots + a_N(s)b_1(s)\dots b_{N-1}(s)} \end{aligned}$$

Note: This identity is based on conductance and the observation that, e.g.,

$$\frac{1}{a} \parallel \frac{1}{b} \parallel \frac{1}{c} = \frac{1}{a+b+c}$$

In our case, we have $z_1 = R + \frac{1}{sC} = \frac{1+sRC}{sC}$

$$z_2 = \frac{1+sRC}{0.4}$$

$$z_3 = sL = \frac{sL}{1}$$

Using the identity, $\underbrace{z_1 \parallel z_2 \parallel z_3}_{Z_{Tot}} = \frac{(1+sRC)^2 sL}{sC(1+sRC)sL + 0.4(1+sRC)sL + (1+sRC)^2}$

After cancellation of $1 + sRC$:

$$z_{Tot} = \frac{(1 + sRC) sL}{s^2 LC + 0.4 sL + (1 + sRC)}$$

Thus, we have

$$\begin{aligned} V_o(s) &= \frac{I(s)}{z_{Tot}} z_{Tot}(s) = \left(\frac{15A}{s} + \frac{i_L(0^-)}{s} + \frac{v_C(0^-)}{s} \frac{sC(1 - 0.4R)}{1 + sRC} \right) \\ &\quad \cdot \frac{(1 + sRC) sL}{s^2 LC + 0.4 sL + 1 + sRC} \\ &= 15A \cdot \frac{L(1 + sRC)}{s^2 LC + 0.4 sL + 1 + sRC} \\ &\quad - i_L(0^-) \frac{L(1 + sRC)}{s^2 LC + 0.4 sL + 1 + sRC} \\ &\quad + v_C(0^-) \frac{C(1 - 0.4R) sL}{s^2 LC + 0.4 sL + 1 + sRC} \end{aligned}$$

Note: we retain the terms for each original source and initial condition.

Now we divide the numerators and denominators by LC to get denominators with the coefficient of s^2 equal to unity.

$$\begin{aligned} V_o(s) &= \frac{15A (1 + sRC)/C}{s^2 + (0.4/C + R/L) s + 1/LC} \\ &\quad - \frac{i_L(0^-) (1 + sRC)/C}{s^2 + (0.4/C + R/L) s + 1/LC} \\ &\quad + \frac{v_C(0^-) (1 - 0.4R) s}{s^2 + (0.4/C + R/L) s + 1/LC} \end{aligned}$$

We find roots of the denominators:

$$s^2 + (0.4/C + R/L)s + 1/LC = s^2 + (0.4/0.2 + 1.6/0.2)s + 1/(0.2)(0.2)$$

$$= s^2 + 10s + 25 = (s+5)^2$$

Other numerical values we need:

$$1 + sRC = 1 + s(1.6)(0.2) = 1 + s \cdot 8/25$$

$$1 - 0.4R = 1 - 0.4(1.6) = 9/25$$

We now use partial fractions.

$$\frac{(1 + sRC)/C}{s^2 + (0.4/C + R/L)s + 1/LC} = \frac{1 + s \cdot 8/25}{(s+5)^2 (0.2)} = \frac{5K_1}{(s+5)^2} + \frac{5K_2}{s+5}$$

$$\text{where } K_1 = \left. \frac{(s+5)^2 (1 + s \cdot 8/25)}{(s+5)^2} \right|_{s=-5} = 1 - 40/25 = -3/5$$

$$K_2 = \left. \frac{d}{ds} (1 + s \cdot 8/25) \right|_{s=-5} = \frac{8}{25}$$

For the $v_C(0^-)$ term:

$$\frac{(1 - 0.4R)s}{s^2 + (0.4/C + R/L)s + 1/LC} = \frac{(9/25)s}{(s+5)^2} = \frac{K_3}{(s+5)^2} + \frac{K_4}{s+5}$$

$$\text{where } K_3 = \left. \frac{(s+5)^2 (9/25)s}{(s+5)^2} \right|_{s=-5} = -9/5$$

$$K_4 = \left. \frac{d}{ds} (9/25)s \right|_{s=-5} = 9/25$$

Using $i_L(0^-) = 5A$ and $v_C(0^-) = 12V$ we have a partial fraction expression for $V_o(s)$:

$$V_o(s) = 15A \cdot \left[\frac{-3}{(s+5)^2} + \frac{8/5}{s+5} \right]$$

$$-5A \left[\frac{-3}{(s+5)^2} + \frac{8/5}{s+5} \right]$$

$$+12V \left[\frac{-9/5}{(s+5)^2} + \frac{9/25}{s+5} \right]$$

We use $\mathcal{L}^{-1} \left\{ \frac{1}{(s+5)^2} \right\} = te^{-5t}$ and $\mathcal{L}^{-1} \left\{ \frac{1}{s+5} \right\} = e^{-5t}$

to find $v_o(t)$:

$$\begin{aligned} v_o(t) = & -45te^{-5t} + 24e^{-5t} \\ & +15te^{-5t} - 8e^{-5t} \\ & - 21.6te^{-5t} + 4.32e^{-5t} \quad V \end{aligned}$$