

Peak amplitude of v_g is $150\sqrt{2}$ V with period $200\pi \mu\text{s}$.

Note: $\omega = 2\pi f$ $f = 1/T$ $T = \text{period}$

$$\therefore \omega = \frac{2\pi}{T} = \frac{10\text{K/s}}{2\pi \cdot 100\mu\text{s}} = 10\text{K/s}$$

- a) Calculate the average power delivered to the load when $R_o = 10\Omega$ and $L_o = 6\text{mH}$.

sol'n: $S = P + jQ = V_{\text{eff}} I_{\text{eff}}^*$ where eff \equiv rms
 $*$ = complex conjugate

$$\left. \begin{aligned} P &= |I_{\text{eff}}|^2 R \\ Q &= |I_{\text{eff}}|^2 X \end{aligned} \right\} \text{for } z = R + jX$$

So we need to find I_{eff} .

$$I_{\text{eff}} = \frac{V_{\text{eff}}}{R_o + j\omega L_o}$$

$$V_{\text{eff}} = V_{g\text{eff}} \cdot \frac{(R_o + j\omega L_o) \parallel -j/\omega C}{R_o + j\omega L_o \parallel -j/\omega C + 300\Omega}$$

$$V_{\text{eff}} = V_{g\text{eff}} \frac{(R_o + j\omega L_o) \cdot \frac{-j/\omega C}{R_o + j\omega L_o - j/\omega C}}{(R_o + j\omega L_o) \cdot \frac{-j/\omega C}{R_o + j\omega L_o - j/\omega C} + 300\Omega}$$

$$\therefore I_{\text{eff}} = V_{g\text{eff}} \frac{-j/\omega C}{R_o + j\omega L_o - j/\omega C} \frac{(R_o + j\omega L_o) (-j/\omega C)}{R_o + j\omega L_o - j/\omega C} + 300\Omega$$

mult top & bottom by $R_o + j(\omega L_o - 1/\omega C)$

$$I_{\text{eff}} = \frac{V_{g \text{ eff}} (-j/\omega C)}{(R_0 + j\omega L_0)(-j/\omega C) + 300 \Omega (R_0 + j\omega L_0 - j/\omega C)}$$

$$I_{\text{eff}} = \frac{V_{g \text{ eff}}}{R_0 + j\omega L_0 + 300 \Omega \left(\frac{\omega C R_0}{-j} + \frac{j\omega L_0 \omega C}{-j} + 1 \right)}$$

$$I_{\text{eff}} = \frac{V_{g \text{ eff}}}{R_0 + j\omega L_0 + 300 \Omega (j\omega C R_0 - \omega^2 L_0 C + 1)}$$

We can use this general formula for $R_0 = 10 \Omega$, $L_0 = 6 \text{ mH}$.

$$\omega L_0 = 10 \text{ k} \cdot 6 \text{ m} = 60 \Omega \quad \omega^2 L_0 C = 60 \Omega \cdot 10 \text{ m} / \Omega = 0.6$$

$$\omega C = 10 \text{ k} \cdot 1 \mu = 10 \text{ m} / \Omega$$

$$V_{g \text{ eff}} = \frac{150 \sqrt{2}}{\sqrt{2}} = 150 \text{ V (rms)}$$

$$\therefore I_{\text{eff}} = \frac{150 \text{ V (rms)}}{10 + j60 + 300(j10 \text{ m} \cdot 10 - 0.6 + 1)}$$

$$= \frac{150 \text{ V (rms)}}{10 - 180 + 300 + j(60 + 30)}$$

$$= \frac{150 \text{ V (rms)}}{130 + j90}$$

$$P = |I_{\text{eff}}|^2 \cdot R_0 = \frac{|150 \text{ V (rms)}|^2}{|130 + j90|^2} \cdot 10 \Omega$$

$$= \frac{|15|^2}{|13 + j9|^2} \cdot 10 \text{ W} = \frac{225 \cdot 10 \text{ W}}{169 + 81} = \frac{225 \cdot 10}{250} = 9 \text{ W}$$

Optional:

b) Determine R_0 and L_0 for max power being transferred to R_0 if $0 \leq R_0 \leq 20 \Omega$ and $1 \leq L_0 \leq 8 \text{ mH}$.

sol'n: max power transfer when $Z_L = Z_{\text{Th}}^*$

If that is not possible, we make X_L as close to $-X_{\text{Th}}$ as possible, and (after that is done) we make R_L as close to $\sqrt{R_{\text{Th}}^2 + (X_L + X_{\text{Th}})^2}$ as possible.

We find Thevenin equivalent of circuit with no load.

$$V_{Th} = \text{open circuit } V = V_g \cdot \frac{-j/\omega C}{-j/\omega C + 300\Omega}$$

Use rms V from now on:

$$V_{Theff} = V_{g\text{eff}} \frac{1}{1 + j\omega C \cdot 300\Omega} = \frac{150 \text{ V (rms)}}{1 + j10\text{m}/\Omega \cdot 300\Omega} = \frac{150 \text{ V (rms)}}{1 + j3}$$

$Z_{Th} = Z$ seen looking in from Z_L terminals with $V_g = 0$

$$= 300 \parallel -j/\omega C = \frac{300 \cdot -j/10\text{m}}{300 - j/10\text{m}} \Omega = \frac{300}{\frac{10\text{m} \cdot 300 + 1}{-j}}$$

$$= \frac{300}{1 + j3} \Omega = \frac{300(1 - j3)}{10} = 30(1 - j3) = 30 - j90 \Omega$$

$$Z_{Th} = 30 - j90 \Omega$$

$$R_{Th} = 30 \quad -X_{Th} = 90 \Omega$$

So we desire $\omega L = 90 \Omega$ or $L = \frac{90}{\omega} = \frac{90}{10\text{k}} = 9 \text{ mH}$

Closest allowed value is 8mH for L_0 .

Then we want $R_L = \sqrt{R_{Th}^2 + (X_L + X_{Th})^2}$

$$(X_L + X_{Th})^2 = (\omega \cdot 8 \text{ mH} + -90)^2 = (-10)^2 = 100 \Omega^2$$

$$\text{want } R_L = \sqrt{30^2 + 100} = \sqrt{1\text{K}} = 31.6 \Omega$$

Closest allowed value is 20Ω for R_L .

c) Find ave power for (b). Compare to answer for (a).

Sol'n: $\omega L_0 = 80 \Omega \quad \omega C R_0 = 10\text{m}/\Omega \cdot 20\Omega = 0.2$

$$\omega^2 L_0 C = 80 \cdot 10 \text{ m} = 0.8$$

$$\therefore I_{\text{eff}} = \frac{150 \text{ V (rms)}}{20 + j80 + 300(j0.2 - 0.8 + 1)} \quad (\text{using formula from part 'a'})$$

$$= \frac{150 \text{ V (rms)}}{20 + 60 + j(80 + 60)} = \frac{150 \text{ V (rms)}}{80 + j140} = \frac{15 \text{ V (rms)}}{8 + j14}$$

$$P = |I_{\text{eff}}|^2 \cdot R_0 = \frac{|15|^2}{|8 + j14|^2} \cdot 20 \text{ W} = \frac{225}{260} \cdot 20 \text{ W}$$

$$P = \frac{225 \text{ W}}{13} = 17.3 \text{ W} \quad \text{which is } > 9 \text{ W from (a).}$$

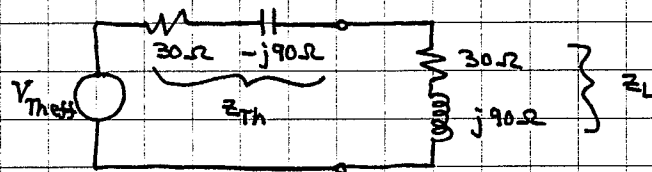
We expected larger P since R_0, L_0 were optimized within ranges given, and R_0, L_0 for part 'a' were in those ranges, too.

d) If no constraints on R_0, L_0 , find optimal R_0, L_0 pwr xfer.

sol'n: We want $Z_L = Z_{\text{Th}}^* = 30 + j90 \Omega$

$$\therefore R_0 = 30 \Omega \quad \text{and} \quad \omega L = 90 \Omega \Rightarrow L = 9 \text{ mH}$$

With $Z_L = Z_{\text{Th}}^*$ we have equiv circuit:



$$\text{So } I_{\text{eff}} = \frac{V_{\text{Th eff}}}{30 - j90 + 30 + j90 \Omega} = \frac{150 \text{ V (rms)}}{60 \Omega} = \frac{5}{2(1 + j3)}$$

$$P = |I_{\text{eff}}|^2 R_0 = \left(\frac{5}{2}\right)^2 \frac{1}{1^2 + 3^2} \cdot 30 \text{ W} = 18.75 \text{ W}$$

e) What are optimal R_0, L_0 for max pwr xfer in (d)? sol'n: $R_0 = 30 \Omega$
see (d) $\Rightarrow L_0 = 9 \text{ mH}$

f) Is pwr in (d) $>$ pwr in (c)? Yes, as expected.