

- Given:
- phase V of ideal balanced 3-phase Y-source = 4.8kV
  - source is connected to balanced Y-load by:
  - distribution line with  $z = 2 + j16 \Omega$ /phase
  - load  $z = 190 + j40 \Omega/\phi$  (ie. per phase)
  - phase sequence is acb (for source)
  - a-phase is reference

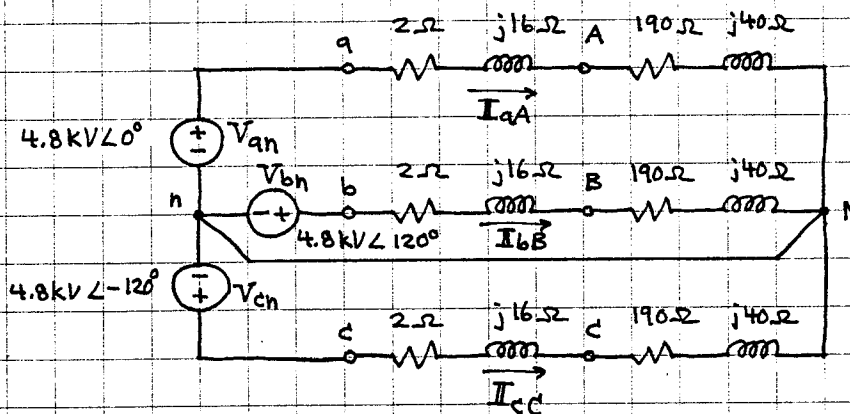
- Specify:
- the 3 line currents
  - " " " voltages at source
  - " " phase " " load
  - " " line " " "

ans: a)  $I_{aA} = 24 \angle -16.3^\circ \text{ A}$       b)  $V_{ab} = 4800\sqrt{3} \angle -30^\circ \text{ V}$   
 $I_{bB} = 24 \angle 103.7^\circ \text{ A}$        $V_{bc} = 4800\sqrt{3} \angle 90^\circ \text{ V}$   
 $I_{cC} = 24 \angle -136.3^\circ \text{ A}$        $V_{ca} = 4800\sqrt{3} \angle -150^\circ \text{ V}$

c)  $V_{AN} = 4660 \angle -4.4^\circ \text{ V}$       d)  $V_{AB} = 8070 \angle -34.4^\circ \text{ V}$   
 $V_{BN} = 4660 \angle 115.6^\circ \text{ V}$        $V_{BC} = 8070 \angle 85.6^\circ \text{ V}$   
 $V_{CN} = 4660 \angle -124.4^\circ \text{ V}$        $V_{CA} = 8070 \angle -154.4^\circ \text{ V}$

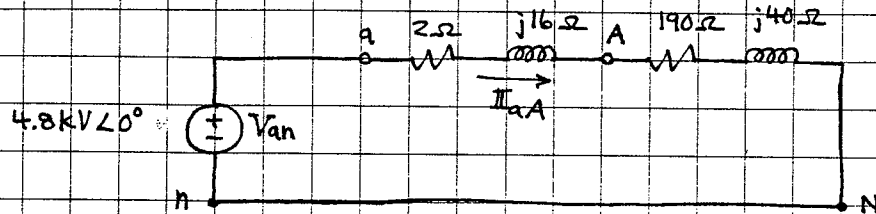
sol'n: a) acb  $\Rightarrow$  negative phase sequence  
 $\therefore$  b or B signals are obtained from a or A signals by adding  $120^\circ$   
 c or C signals " " " a or A  
 " " adding  $-120^\circ$  (or subtracting  $+120^\circ$ )

System diagram: (since a-phase is ref, use  $0^\circ$  for  $V_{an}$ )



Note: No current flows in nN (grd) connection for balanced 3-phase system.

We can solve for all the requested values by employing a single-phase model:



Now for definitions:

line  $\equiv$  distribution line connecting a to A.

(In real life a high voltage line connecting a generator at Hoover Dam <sup>ultimately</sup> to a wall socket in your house.

These are the high-voltage lines we see crossing the desert:



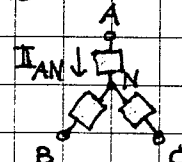
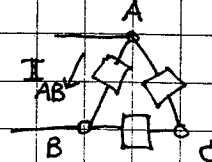
line current  $\equiv$  current flowing in the distribution line

line voltage  $\equiv$  the voltage difference across a pair of distribution lines.

(We can measure this at the source such as Hoover Dam or at the load such as a large motor in a factory)

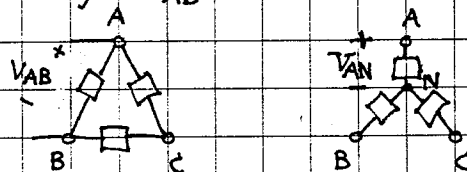
phase current  $\equiv$  current flowing thru one leg of a  $\Delta$  or Y configuration.

For  $\Delta$  config. we have, e.g. phase current  $I_{AB}$ . For Y it's  $I_{AN}$ .



phase voltage  $\equiv$  voltage across an leg of a  $\Delta$  or Y configuration.

For  $\Delta$  we have, e.g. difference voltage  $V_{AB}$ . For Y it's  $V_{AN}$ .



Thus, line current is  $I_{aA}$  for 1<sup>st</sup> phase, (i.e. 'a' phase).

Using single-phase model, we just apply standard circuit eq'ns:

$$I_{aA} = \frac{V_{an}}{Z_{tot}} = \frac{4.8kV \angle 0^\circ}{2 + j16 + 190 + j40} A = \frac{4.8kV \angle 0^\circ}{192 + j56} A$$

$$I_{aA} = \frac{4.8kV \angle 0^\circ}{200 \angle 16.3^\circ} A = 24 \angle -16.3^\circ A$$

We obtain the other line currents by shifting  $\pm 120^\circ$ :

$$I_{bB} = I_{aA} \cdot 1 \angle +120^\circ = 24 \angle 103.7^\circ A$$

$$I_{cC} = I_{aA} \cdot 1 \angle -120^\circ = 24 \angle -136.3^\circ A$$

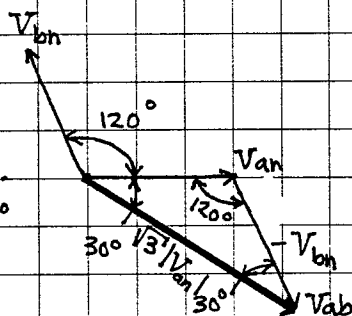
b) Line voltage at source is  $V_{ab} \equiv V_{an} - V_{bn}$ .

Use phasor diagram and fact that  $V_{bn} = V_{an} \cdot 1 \angle 120^\circ$ :

$V_{ab} \equiv V_{an} - V_{bn}$   
gives  $V_{ab}$  = long side of isosceles triangle.

$\angle$  relative  $V_{an} = -30^\circ$

$$|V_{ab}| = \sqrt{3} |V_{an}|$$



Note: for positive phase sequence we would get  $+30^\circ$  for  $\angle V_{ab}$  relative to  $\angle V_{an}$ .

From diagram, we have  $V_{ab} = V_{an} \cdot \sqrt{3} \angle -30^\circ$ .

Using this result and  $\pm 120^\circ$  phase shifts gives:

$$V_{ab} = 4.8 \text{ kV} \angle 0^\circ \cdot \sqrt{3} \angle -30^\circ = 4800 \sqrt{3} \angle -30^\circ \text{ V}$$

$$V_{bc} = 4800 \sqrt{3} \angle -30^\circ + 120^\circ = 4800 \sqrt{3} \angle 90^\circ \text{ V}$$

$$V_{ca} = 4800 \sqrt{3} \angle -30^\circ - 120^\circ = 4800 \sqrt{3} \angle -150^\circ \text{ V}$$

c) Since we have a Y load, the phase voltages at the load are  $V_{AN}$ ,  $V_{BN}$ ,  $V_{CN}$ .

To find  $V_{AN}$ , we use  $V_{an}$  and V-divider:

$$V_{AN} = V_{an} \cdot \frac{190 + j40}{2 + j16 + 190 + j40} = V_{an} \frac{190 + j40}{192 + j56}$$

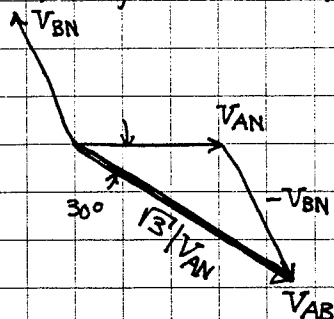
$$= 4800 \angle 0^\circ \cdot \frac{194 \angle 11.9^\circ}{200 \angle 16.3^\circ} = 4800 \cdot \frac{194}{200} \angle 0^\circ + 11.9^\circ - 16.3^\circ \text{ V}$$

$$= 4.66 \text{ kV} \angle -4.4^\circ$$

$$V_{BN} = V_{AN} \cdot 1 \angle 120^\circ = 4.66 \text{ kV} \angle 115.6^\circ$$

$$V_{CN} = V_{AN} \cdot 1 \angle -120^\circ = 4.66 \text{ kV} \angle -124.4^\circ$$

d) Line voltages at load are  $V_{AB} = V_{AN} - V_{BN}$ ,  $V_{BC}$ ,  $V_{CA}$ .



As with  $V_{ab}$  vs  $V_{an}$ , we have  $V_{AN} = V_{AN} \cdot \sqrt{3} \angle -30^\circ$ .

$$\therefore V_{AB} = 4.66 \text{ kV} \angle -4.4^\circ \cdot \sqrt{3} \angle -30^\circ$$

$$= 8070 \angle -34.4^\circ \text{ V}$$

$$V_{BC} = 8070 \angle -34.4^\circ + 120^\circ = 8070 \angle 85.6^\circ \text{ V}$$

$$V_{CA} = 8070 \angle -154.4^\circ \text{ V}$$