

Chapter 3 Notes

(27-1)

Sample Problem on Rectangular Waveguide (Similar to Prob. 15 of HW; also see Ex. 3.1 of the Text)

- a. Select a rectangular waveguide capable of propagating signals at 10 GHz.

From the Table of commercially available rectangular waveguides on p. (27) of my notes, any of the following three waveguides may be used:

WR 112

$$f_d = \frac{c}{2a} \\ \text{TE}_{10} \\ 5.259 \text{ GHz}$$

Recommended frequency range
for TE_{10} mode

7.05 - 10.0 GHz

WR 90

$$6.557$$

8.20 - 12.4 GHz

WR 75

$$7.868$$

10.00 - 15.00 GHz

Of the three waveguides WR 90 is the best compromise in that it has lower attenuation than WR 75 (which is the smallest waveguide for this frequency) and is not as bulky as WR 112.

- b. List in ascending order the frequencies of the five lowest order modes.

From Eq. 3.84 of the Text

$$f_{cmn} = \frac{c}{2} \sqrt{\frac{m^2}{a^2} + \frac{n^2}{b^2}}$$

For an air-filled WG $c_e = c = 3 \times 10^8 \text{ m/sec}$, $a = 0.9'' = 2.286 \times 10^{-2} \text{ m}$; $b = 0.4'' = 1.016 \times 10^{-2} \text{ m}$

For WR 90: $a = 0.9'' = 2.286 \times 10^{-2} \text{ m}$; $b = 0.4'' = 1.016 \times 10^{-2} \text{ m}$

In order of ascending cut-off frequencies, the five lowest cut-off frequency modes are:

$$f_c$$

TE_{10} $m=1$
 $n=0$

$$\frac{c}{2a} = 6.557 \text{ GHz}$$

TE_{20} $m=2$
 $n=0$

$$\frac{c}{a} = 13.114 \text{ GHz}$$

TE_{01} $m=0$
 $n=1$

$$\frac{c}{b} = 14.764 \text{ GHz}$$

$\text{TE}_{11} \}$ $m=1$
 $\text{TM}_{11} \}$ $n=1$

$$\frac{c}{2} \sqrt{\frac{1}{a^2} + \frac{1}{b^2}} = 16.156$$

- c. For the lowest order (single mode) propagation of TE_{10} mode

$$1.25 \frac{c}{2a} \leq f \leq 0.95 f_c \Rightarrow 8.2 \leq f \leq 12.4 \text{ GHz}$$

c. $\left| \lambda_g \right| = \frac{2\pi}{\beta} = \frac{\lambda_0 / \sqrt{\epsilon_r}}{\sqrt{1 - (\frac{f_c^2}{f^2})}} = \frac{3}{\sqrt{1 - (\frac{6.557}{10})^2}} = 3.975 \text{ cm}$

$$\left| \lambda_g \right|_{10 \text{ GHz}} = \frac{4}{\sqrt{1 - (\frac{6.557}{7.5})^2}} = 8.24 \text{ cm}$$

d. From Eq. 3-96 on p. 111 of the Text (see also Eqs. on p. 126 of my notes)

$$\left| \alpha_c \right| = \frac{R_s}{b} \gamma \left[\frac{f_c}{f} \frac{\left[\frac{f^2}{f_c^2} + \frac{2b}{a} \right]}{\sqrt{\frac{f^2}{f_c^2} - 1}} \times 8.686 \right] \xrightarrow{\text{to convert nepers/m into dB/m}}$$

Assuming Aluminum to be the material of the waveguide

$$R_s = 1.988 \sqrt{\frac{f \text{ MHz}}{0}} \quad \text{from p. 27 of the Text}$$

$$= 1.018 \times 10^2 \Omega$$

$$\left| \alpha_c \right| = 0.1337 \text{ dB/m}$$

e. power lost in a waveguide for a waveguide length of 3m

$$\text{Attenuation} = 0.1337 \times 3 \approx 0.4 \text{ dB}$$

$$\text{Power output} = P_{in} \frac{-0.4}{10} = 0.912 \text{ P}_{in}$$

Thus 8.8% of the input power is lost over a WG length of 3 m.

f. From Eq. 3.92 of the Text (see also Eq. on p. 126 of my notes)

$$P_{10} = \frac{ab}{4Z_{TE}} (E_{max})^2$$

For an input power of 100 kW at 10 GHz (air-filled WG)

$$Z_{TE} = \frac{\eta_e}{\sqrt{1 - (\frac{f_c^2}{f^2})}} = 499.5 \Omega \quad (3.92)$$

$$E_{max} = 9.275 \times 10^3 \text{ V/cm} \quad \begin{matrix} \text{dry air} \\ \text{(this is less than the breakdown field strength of } 29000 \text{ V/cm)} \end{matrix}$$

g. $P_{BD} = 3.6 \left| a \right|_{\text{inch}} \left| b \right|_{\text{inch}} \sqrt{1 - (\frac{f_c^2}{f^2})} = 0.978 \text{ MW}$

Ex. Find the load impedance if VSWR and location of Voltage maximum (or minimum) is known.

$$\text{say } \text{VSWR} = 2.0 \quad |P| \rightarrow |S_{11}| = \frac{\text{VSWR}-1}{\text{VSWR}+1}$$

location of Voltage maximum = $0.3 \lambda_g$ from the load.
 (impedance ~~maximum~~) $1.1925 \text{ cm} @ 10 \text{ GHz}$

From Smith chart $\underline{Z}_L = 0.56 - j 0.24$

$$\underline{S}_L = 0.32 e^{-j14^\circ} \quad \leftarrow \frac{\underline{Z}_L - 1}{\underline{Z}_L + 1} \quad \begin{array}{l} \text{an open ended WG} \\ \text{acting as a radiator} \\ \text{presents an effective load} \\ \text{to the WG.} \end{array}$$

$$\begin{aligned} Z_L &= \underline{Z}_L Z_{TE} = 499.5 (0.56 - j 0.24) \\ &= 279.7 - j 119.9 \Omega \end{aligned}$$

Ex. calculate the magnitude of \vec{E} at the ^{load or the} open end of the WG

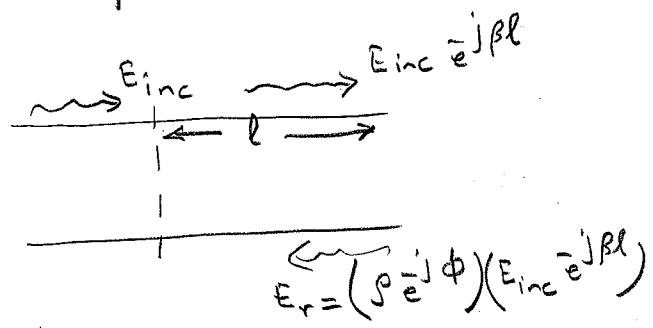
$$\text{say } l = 0.3 \lambda_g$$

$$\text{for } P_{in} = 100 \text{ kW}$$

$$E_{inc} = 9.275 \times 10^5 \text{ V/m peak}$$

$$\vec{E} \Big|_{\text{open end}} = E_{inc} e^{-j\beta l} \left[1 + |P| e^{-j\phi} \right]$$

$$\begin{aligned} \vec{E} \Big|_{\text{open end}} &= E_{inc} \left| 1 + 0.32 e^{-j14^\circ} \right| \\ &= 0.7646 E_{inc} = 7.09 \times 10^5 \text{ V/m peak} \end{aligned}$$



"SMITH CHART"

