

To create an unconventional root locus plot:

1. Determine the gain factor if it can be adjusted, and make it part of the open-loop transfer function, $G(s)$. Hold it constant at some number.
2. Determine the denominator of the closed-loop transfer function, $H(s)$. Let's call it $D_H(s)$.
3. Rearrange $D_H(s)$ into this form: $D'(s) + x \cdot N'(s)$ where x is the variable for which you want to draw the root locus. Notice that x occupies exactly the same position the gain would normally occupy. Normal: $D_G(s) + k \cdot N_G(s)$
 Note: If you cannot rearrange $D_H(s)$ into this form, then you cannot use this method to create an root locus plot for the variable x . Now: $D'(s) + x \cdot N'(s)$
4. Now simply draw a root locus as though $D'(s)$ was the open-loop denominator and $N'(s)$ was the open-loop numerator.

Root Locus Design

PI To eliminate steady-state error (for constant inputs) & perfect rejection of constant disturbances
 Add pole at 0 and zero at close by

LAG An alternative is a Lag Compensator, with a pole near the origin and a zero a little farther away.

PD or PID To Improve the dynamic response, add a zero to affect angles.

LEAD An alternative to the differentiator is a Lead Compensator with a zero and a pole much farther left.

Root Locus Design Crib Sheet

Using 2nd-order approximation: $\frac{N(s)}{(s+a)^2 + b^2} = \frac{N(s)}{s^2 + 2 \cdot a \cdot s + a^2 + b^2} = \frac{N(s)}{s^2 + 2 \cdot \zeta \cdot \omega_n \cdot s + \omega_n^2}$

$\omega_n^2 = a^2 + b^2$ $\omega_n =$ natural frequency

$\zeta = \frac{a}{\omega_n} = \frac{a}{\sqrt{a^2 + b^2}} =$ damping factor $\zeta = \sin\left(\text{atan}\left(\frac{a}{b}\right)\right)$

Overshoot: $OS = e^{-\frac{\pi \cdot a}{b}}$ $\%OS = 100\% \cdot e^{-\frac{\pi \cdot a}{b}}$ $\frac{a}{b} = \frac{\ln(OS)}{-\pi}$

2% settling time: $T_s = \frac{4}{a} = \frac{4}{\zeta \cdot \omega_n}$ $\%OS = 100\% \cdot e^{\frac{-\zeta \cdot \pi}{\sqrt{1-\zeta^2}}}$ $\zeta = \frac{-\ln(OS)}{\sqrt{\pi^2 + (\ln(OS))^2}}$
 Weird forms from Nise book

Static error constant (position): $K_p = \lim_{s \rightarrow 0} K \cdot C(s) \cdot G(s)$ $e_{\text{step}(\infty)} = e_{\text{step}} = \frac{1}{1 + K_p}$

Lag compensation improves K_p , K_v and K_a by $\frac{z_c}{p_c}$ IE: $K_{pc} \simeq K_{puc} \cdot \frac{z_c}{p_c}$

angle of constant damping line: $90\text{-deg} + \text{atan}\left(\frac{a}{b}\right)$

Bode Plots

Sample transfer function:
$$P(s) = K \cdot \frac{(s+z_1) \cdot (s+z_2)}{s \cdot (s+p_1) \cdot (s+p_2)^2}$$

Replace all s's with blanks:
$$P(_) = K \cdot \frac{(-+z_1) \cdot (-+z_2)}{- \cdot (-+p_1) \cdot (-+p_2) \cdot (-+p_2)}$$

Initial magnitude =
$$K \cdot \frac{z_1 \cdot z_2}{(j \cdot \omega_{\text{start}}) \cdot p_1 \cdot (p_2) \cdot (p_2)}$$

ω 's in num --> +20dB/dec each , $j \Rightarrow +90^\circ$, $- \Rightarrow +180^\circ$
 ω 's in den --> -20dB/dec each , $j \Rightarrow -90^\circ$, $- \Rightarrow -180^\circ$

Cross out each pole or zero in turn & replace with $j\omega$
$$K \cdot \frac{(-+z_1) \cdot (-+z_2)}{(j\omega) \cdot (j\omega + \mathbf{X}_1) \cdot (-+p_2) \cdot (-+p_2)}$$

zeros turn up the slope --> +20dB/decade
 poles turn down the slope --> -20dB/decade

zeros increase the phase angle --> +90deg
 poles decrease the phase angle --> -90deg

Draw a smooth line through the bode plots to estimate the actual magnitude and phase.

Actual magnitude: -3dB at single poles -6dB at double poles etc..
 +3dB at single zeros +6dB at double zeros Magnitude effects extend about 1 decade fore and aft.

Angle effects extend about 1.5 decade fore and aft. It is helpful to draw a line from 1 decade before to 1 decade after.

$$(s+a)^2 + b^2 = s^2 + 2 \cdot a \cdot s + a^2 + b^2$$

$$= s^2 + 2 \cdot \zeta \cdot \omega_n \cdot s + \omega_n^2$$

natural frequency $\omega_n = \sqrt{a^2 + b^2}$

damping factor $\zeta = \frac{a}{\omega_n}$

max at approx ω_n , $\frac{1}{2 \cdot \zeta}$

in dB: $20 \cdot \log\left(\frac{1}{2 \cdot \zeta}\right)$

